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THESIS

A THREE-DIMENSIONAL TRANSONIC, POTENTIAL FLOW
COMPUTER PROGRAM, ITS CONVERSION TO IBM
FORTRAN AND UTILIZATION

by

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December 1983

Thesis Advisor:

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A Three-Dimensional Transonic, Potential Flow Computer
Program, Its Conversion to IBM Fortran and Utilization

by

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Submitted in partial fulfillment of the
requirements for the degree of

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ABSTRACT

This thesis describes the conversion of a computer program from Fortran IV for the NOS 1.2 operating system of the CYBER 175 or CDC 6600 computer to Fortran IV compatible with the Naval Postgraduate School IBM 3033 system. The converted program, called FLO27, calculates the inviscid, three-dimensional transonic potential flow over wings or wing-body combinations. The data input to FLO27 is extensive; therefore, an interactive program was developed to aid the user in building the required input data file.

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I. INTRODUCTION

In the Aeronautical Engineering curriculum graduate level aerodynamics course, AE-4501, the students are exposed to two computer programs. One of these, prepared by the Douglas Aircraft Company, analyzes the potential flow around three-dimensional wings but is limited to incompressible flow [Ref. 1]. The other program, prepared by Cebeci, calculates the friction drag for two dimensional incompressible flow over airfoils [Ref. 2]. A serious defect of these programs is that they are not state-of-the-art computer programs. The Douglas program does not consider the effects of compressibility and the boundary layer program, in addition to being restricted to incompressible flow, does not predict the laminar to turbulent transition point.

A. BACKGROUND

In 1980 the Department of Aeronautics at the Naval Postgraduate School acquired an intricate computer program recently developed by the Boeing Commercial Airplane Company. This state-of-the-art program calculates three-dimensional transonic flow over wings and bodies in

both the outer-inviscid flow region governed by the transonic potential equation and the thin layer in which the first order, compressible boundary layer equations are assumed to be valid.

The Boeing program as received was designed to be executed on a CDC 6600 or a CYBER 175 computer and was written using CDC FORTRAN IV extended language. This thesis therefore was primarily concerned with the conversion of the program to FORTRAN IV extended compatible with the Naval Postgraduate School's (NPS) IBM 3033 system. The large modular program was divided so that the potential flow analysis portion could be run separately. Simplified instructions for use of the program were also prepared.

B. VISCOUS/INVISCID SYSTEM OF PROGRAMS

The Viscous/Inviscid Wing System (VIWS) of programs calculates three-dimensional transonic flow over wings and wing body combinations including details of the laminar or turbulent flow in the three-dimensional viscous boundary layer. The flow field is calculated in two overlapping regions: an outer inviscid flow region governed by the transonic potential equation, and a thin boundary layer in which the first order, three-dimensional, compressible

boundary layer equations are assumed to hold and in which the effects of surface heat and mass transfer can be computed. A list of the VIWS of programs is presented in Table I.

TABLE I

Viscous/Inviscid Wing System of Programs

Program Name	Description
F1027	Jameson-Caughey inviscid, transonic wing code
A411IN	Reads geometry & velocity data, constructs coordinate system
VWIN	Potential flow boundary layer interface
A411AC1	Three-dimensional boundary layer program
INTERP	Boundary layer potential flow interface
A411P1 A411D2 A411FS	Graphics display programs

The basic sequence of calculations used by the VIWS to obtain matched viscous and inviscid solutions consists of an iterative loop in which the inviscid outer flow analysis and the boundary layer analysis are performed sequentially. The iterative sequence is continued until either convergence (satisfactory matching) is achieved, or the maximum number of iterations specified by the user has been performed. The VIWS programming sequence is shown schematically in Fig. 1.1.

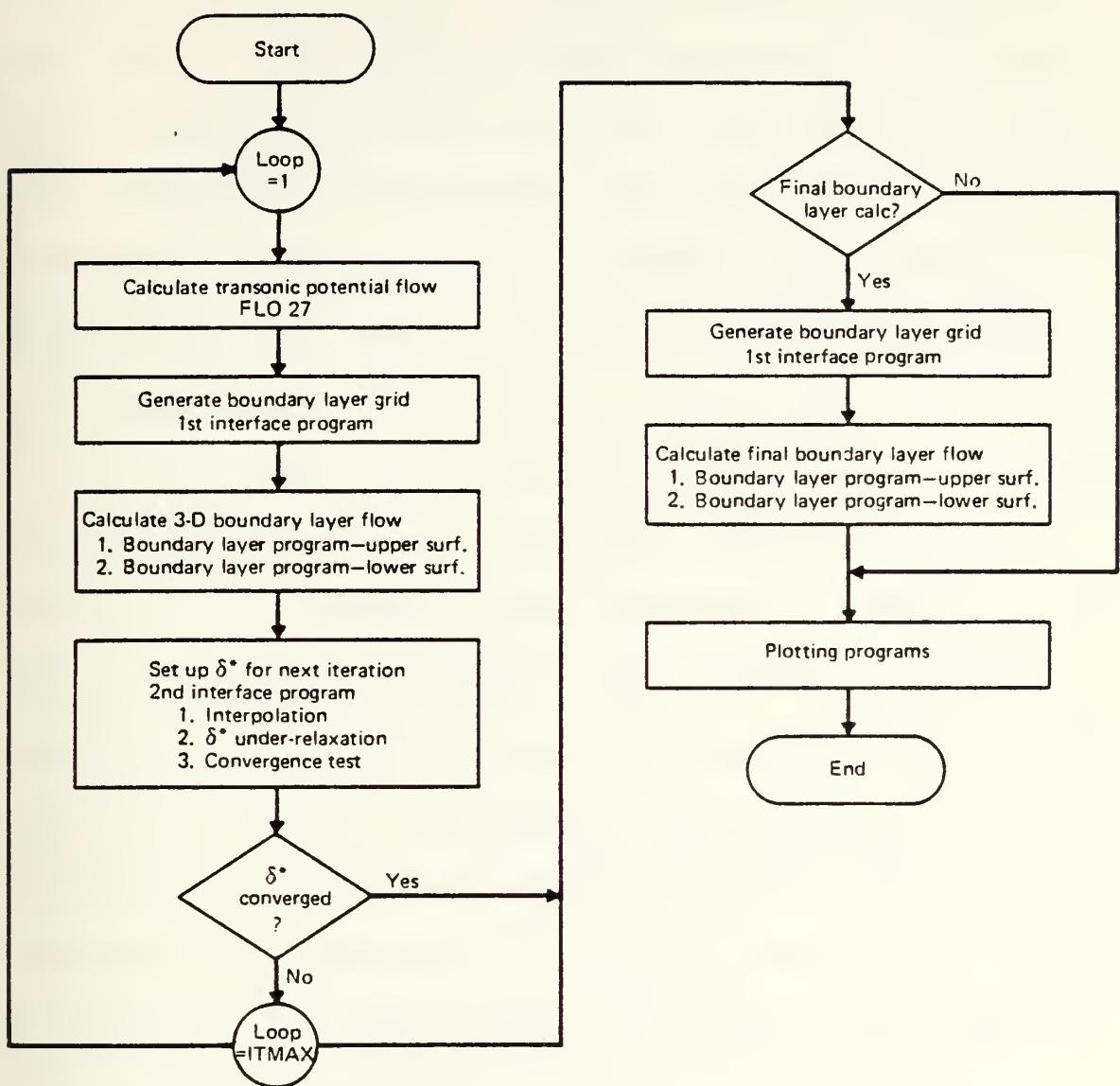


Figure 1.1. Viscous/Inviscid Interaction Procedure

The potential flow is calculated for the bare wing during the first iteration. In subsequent iterations, the effect of the boundary layer flow on the outer inviscid flow is

felt as a modification to the wing shape through the addition of the boundary layer displacement thickness. Convergence is recognized, and the iterations are stopped, when the maximum change between the new and old displacement thickness, expressed as a fraction of the maximum displacement thickness, is less than the convergence tolerance chosen by the user.

The VIWS utilizes the Jameson-Caughey transonic inviscid wing program FLO27, to carry out the potential flow analysis. The boundary layer analysis is performed by a finite difference boundary layer prediction program developed by the Boeing Commercial Airplane Company. The basic theory behind the boundary layer program is contained in [Ref. 3]. A detailed description of the VIWS of programs (excluding the potential flow program FLO27) is contained in [Ref. 4]. A basic guide to the use of the VIWS of programs is contained in [Ref. 5].

III. POTENTIAL FLOW PROGRAM FLO27

Because of the extensive length and number of program modules in the VIWS, the Potential Flow Program, FLO27, was singled out for conversion. It was anticipated that FLO27 would be run separately at first and recombined with the other program modules at some later date when these modules were themselves translated for execution on the IBM 3033 computer.

A. RE-PROGRAMMING

The Potential Flow Program, hereafter called FLO27, was received on magnetic tape and loaded into the IBM 3033 mass storage system using the Job Control Language (JCL) routines presented in Appendix A. The magnetic tape contained twenty (20) total files in which the format was 9 track, 1600 CPI, unlabeled. The card image format for the sixteen (16) program files is 80 characters per record and the four (4) output files contain 150 characters per record. The program and output files on the original CDC tape are listed in Table II.

The FLO27 program was converted to FORTRAN IV extended suitable for execution on the IBM computer using the NPS CDC

TABLE II
CDC Magnetic Tape Files

File/Records	Name	Description
1 / 2356	FLO27	Potential Flow Program
2 / 3194	A411IN	Reads geometry & velocity data constructs coordinate system
3 / 378	VWIN	Potential flow boundary-layer interface
4 / 6611	A411AO1	Three-dimensional boundary layer program
5 / 1977	INTERP	Boundary-layer potential flow interface
6 / 688	A411PS	Streamline plots
7 / 211	A411P1	One-dimensional plots
8 / 586	A411P2	Contour plots
9 / 70	COUPLE	Procedure files
10 / 158	ITER	
11 / 7	DATAIN	
12 / 78	FINAL	
13 / 434	BOEB1	Boeing McLean computer program
14 / 36	CONTPLT	Contour plots
15 / 17	CORDPLT	One-dimensional plots
16 / 40	STREPLT	Streamwise plots
17	OUTF27	Output from FLO27
18	OUTIFC	Output from VWIN
19	OUT411L	Output from boundary-layer, lower surface
20	OUT411U	Output from boundary-layer, upper surface

to IBM conversion guide [Ref. 6]. The first step taken consisted of program compilation using the WATFIV compiler with its extended error messages. The listing which was

produced flagged all areas of the program which required revision. Program changes were accomplished utilizing this WATFIV listing. Some of the more general and repetitive changes are listed in Table III.

TABLE III
FLO27 Re-Programming Changes

CDC Code	IBM Code Change
Variables: FREAD, FREAF, FWRIT, FWRIIF, IREAD, IREAF, IWRIT, IWRIF	Eliminated from program
WRITE(IWRIT,600)	WRITE(6,600)
READ(IREAF,500)	READ(5,500)
READ 7, WRITE 7 or REWIND 7	Changed to READ 14, WRITE 14 or REWIND 14
Call SECOND(T)	Step eliminated
Call SSWITCH(1,ISTOP)	Call SLITET(1,ISTOP)
Delimiter of form *	Replaced by '
Comment cards with *	Replaced by C
LEVEL statement	Step eliminated
If(UNIT(N).GT.0.) GO TC	All of this type eliminated

The most difficult change to make occurred with the CDC Buffer IN or Buffer OUT statements which were used in the program to transfer portions of a three-dimensional array into and out of main memory. The Buffer routines reduce the memory size required to execute the program. This statement type occurred in the main program and several of the subroutines.

The change required to translate this statement is presented below with the CDC code preceding the IBM FORTRAN.

```
BUFFER OUT (N3,1) (G(1,1,1),G(MX,MY,1)) changed to  
WRITE(N3) ((G(I,J,1),I=1,MX),J=1,MY) and  
BUFFER IN (N1,1) (G(1,1,M),G(MX,MY,M)) changed to  
READ(N1,ERR= ) ((G(I,J,M),I=1,MX),J=1,MY)
```

The variable ERR was assigned the GO TO statement number of the UNIT statement immediately following the BUFFER IN line of code. As an example, if the UNIT statement following the BUFFER IN code was - IF(UNIT(N1).GT.0.) GO TO 151, then the number 151 was assigned to variable ERR following the equal sign. All CDC UNIT statements were eliminated from the FLO27 source code per Table II.

In addition to the program changes required to run FLO27 on the IBM computer, several lines of code were added to modify the output format to a more usable form. A subroutine, VERTEC, which calls the Versatec plotter was also added to enhance program usefulness. This plotting routine is user controlled through an input variable and is explained in the next section. The modified FLO27 program source code is presented in Appendix E.

To facilitate program data entry several input variables which had recommended values were initialized to these values within the Main program and the subroutine GEOM. The initialized input variables and their values are presented in Table IV.

TABLE IV
Initialized Input Variables

AREA	VARIABLE NAME	INITIALIZED VALUE
MAIN Prgm.	XSCAL	0.0
	PSCAL	0.0
	FCONT	0.0
	P20	0.7
	P30	1.0
	FSMCO	0.0
	PTMAP	0.0
	BLCP	0.0
	WEIG	1.0
	PTCK	0.0
Subrt. GEOM	FIX	0.0
	YSYM	0.0
	FNB	2.0
	PX	0.0
	PZ	0.0
	TRL	0.0
	SLT	0.0
	XSING	0.0
	YSING	0.0

A complete description of each input variable in Table IV can be found on pages 19 through 23 of [Ref. 5].

B. PROGRAM DESCRIPTION

The FLC27 program is a computer code written to analyze the transonic flow over a wing alone or a wing on a cylindrical fuselage. It uses a finite-volume formulation to solve the exact potential flow equation in conservative form. In the development of the equations, the basic assumptions are; steady flow, no heat or work transfer, isentropic flow, irrotational flow, no body forces and a perfect gas. The velocity vector in cartesian coordinates is

$$\vec{V} = u\hat{i} + v\hat{j} + w\hat{k} \quad (2.1)$$

where u , v and w are the velocity components. The continuity equation, assuming steady flow, is

$$\frac{\partial}{\partial x}(\rho u) + \frac{\partial}{\partial y}(\rho v) + \frac{\partial}{\partial z}(\rho w) = 0 \quad (2.2)$$

Next a velocity potential is introduced such that the velocity components are calculated as the gradient of this potential.

$$u = \phi_x, \quad v = \phi_y, \quad w = \phi_z \quad (2.3)$$

With the introduction of the velocity potential, the continuity equation 2.2 becomes

$$\frac{\partial}{\partial x}(\rho \phi_x) + \frac{\partial}{\partial y}(\rho \phi_y) + \frac{\partial}{\partial z}(\rho \phi_z) = 0 \quad (2.4)$$

Assuming no heat or work transfer, the energy equation can be written as

$$T \left[1 + \frac{(\gamma - 1)}{2} M^2 \right] = T_{\infty} \left[1 + \frac{(\gamma - 1)}{2} M_{\infty}^2 \right] \quad (2.5)$$

The flow is assumed to be uniform in the far field. On the surface of the body, the normal velocity component is zero. The velocities and densities of the near field are normalized using the free stream velocity and density, thus $v_{\infty} = 1$ and $\rho_{\infty} = 1$. Using the assumptions that the flow is isentropic and a perfect gas, the energy equation 2.5 can be shown to be

$$\rho = \left[1 + \frac{(\gamma - 1)}{2} M_{\infty}^2 \left(1 - v^2 \right) \right]^{-\frac{1}{\gamma - 1}} \quad (2.6)$$

With equations 2.5 and 2.6 there are only two unknowns, ϕ and ρ . They can be solved, subject to the boundary condition of flow tangency, using a finite volume technique. The basic numerical scheme for the solution is the

construction of a mesh from small volume elements (cubes) which are packed around the wing or wing-body configuration. The cubes in the computational domain are separately mapped to distorted cubes in the physical domain by independent transformations from local coordinates X, Y and Z to Cartesian coordinates x, y and z. The mesh points are the vertices (corners) of the mapped cubes. The velocity potential and density are calculated at each vertex in the mesh. The pressure distribution can then be calculated from

$$P = \frac{\rho \sigma}{\gamma M_\infty^2} \quad (2.7)$$

In the event that the local flow velocity becomes supersonic and shocks occur, these are handled in the usual manner by insuring that:

- 1) The tangential velocity components are equal on each side of the shock.
- 2) Continuity is maintained by keeping the product of ρu_n constant across the shock (where u_n is the normal velocity component).
- 3) Discontinuous expansions (corresponding to an "expansion shock") are excluded from the flow field.

The assumption of isentropic flow along with the existence of shocks presents a contradiction which can only be resolved by limiting the flow to very weak shocks for which entropy and vorticity generation may be ignored. Thus, solutions will be valid only for subsonic free stream velocities.

The main three-dimensional array containing the potential function data is stored on disk, and special unformatted input/output statements are used to bring planes of data into central computer memory and to store updated planes of data back on the disk. In the construction of the computational coordinate system, a Joukowski transformation is used to transform the cylindrical fuselage to a vertical slit and then a sheared parabolic transformation is used in planes containing the airfoil sections. A detailed mathematical formulation of the potential flow analysis is contained in [Ref. 7].

1. Program Input

The input to FLO27 consists of variables which are read with an 8F10.6 FORMAT. Each input card has a title card which precedes it. This title card contains the input variable name and effectively labels the input data for easy

reference. The title for each input data is placed in the same column as the input data it labels. The title cards are read with a 20A4 FORMAT. All numerical input values are real numbers. The following data deck, listed card by card, is the minimum input data required for a simple wing analysis. Each "card" can be interpreted as one line of data on your terminal. A complete sample data set is presented in Appendix C.

CARD 1 The Run Title (64 characters maximum)

CARD 2 Title card for the input variables

FNX, FNY, FNZ, FMESH and FPILOT

CARD 3

Cols. 1-10 FNX - Number of computational cells in the chordwise direction for the initial mesh.

MAX = $160/2^{**n}$, where n = FMESH - 1. (See Cols. 31-40 for FMESH)

Cols. 11-20 FNY - Number of computational cells in the normal direction from the airfoil surface for the initial mesh.

MAX = $16/2^{**n}$, where n = FMESH - 1.

Cols. 21-30 FNZ - Number of computational cells in the spanwise direction for the initial mesh.

MAX = $32/2^{**n}$, where n = FMESH - 1.

Cols. 31-40 FMESH - Determines the number of times a program generated computational mesh is refined. Enter only 1.0, 2.0 or 3.0 for coarse, medium or fine mesh. If 3.0 is selected the program will calculate flow over the wing for the coarse mesh then half the mesh size (medium), recalculate, then half the mesh again (fine) and do a final potential flow calculation. Output parameters are printed for each mesh size for which calculations were performed.

Cols. 41-50 FPLOT - Output flag

0.0 = Normal output without printer-plot of Cp

1.0 = Normal output with printer-plot of Cp
at each computational mesh point for
each wing section.

2.0 = Normal output with Versatec plots of
Cp versus X/C for each wing section of
the final mesh.

CARD 4 Title card for the input variables

FIT, COVO and P10

CARD 5-M One card for each computational mesh. Total
number of cards equal to M = FMESH.

Cols. 1-10 FIT - A parameter which fixes the maximum number of iterations the program will use to converge the velocity potential to a specified tolerance (COVO). This parameter must be repeated for each mesh refinement.

Cols. 11-20 COVO - Velocity potential convergence criteria. This input variable is also entered for each selected mesh. A value of 0.000001 is recommended.

Cols. 21-30 P10 - This parameter determines the subsonic point relaxation factor for the specified mesh size. A value of less than 2.0 must be entered for each designated mesh. Recommended values are: 1.6 for coarse, 1.3 for medium and 1.2 for the fine mesh.

CARD 6 Title card for the input variables

FMACH, YA, AL and CDO

CARD 7

Cols. 1-10 FMACH - Free stream Mach number

Cols. 11-20 YA - Yaw angle in degrees

Cols. 21-30 AL - Angle of attack in degrees

Cols. 31-40 CDO - Drag coefficient due to skin friction. Unless known, an estimated value of 0.01 is recommended.

CARD 8 Title card for the input variables

ZSYM, FNS, SWEEP, DIHED and FUS

CARD 9

Cols. 1-10 ZSYM - The wing planform symmetry trigger.

0.0 = Yawed wing, has no spanwise symmetry

1.0 = Swept wing, has spanwise symmetry

Cols. 11-20 FNS - This input variable tells the program the total number of wing sections you have selected to define the wing half span. The number must be at least three (3) but not more than eleven (11) sections.

Cols. 21-30 SWEEP - Leading edge sweep angle in degrees.

Cols. 31-40 DIHED - Dihedral angle in degrees. See Fig. 2.1.

Cols. 41-50 FUS - Input the fuselage radius. Enter 0.0 for a wing-alone case.

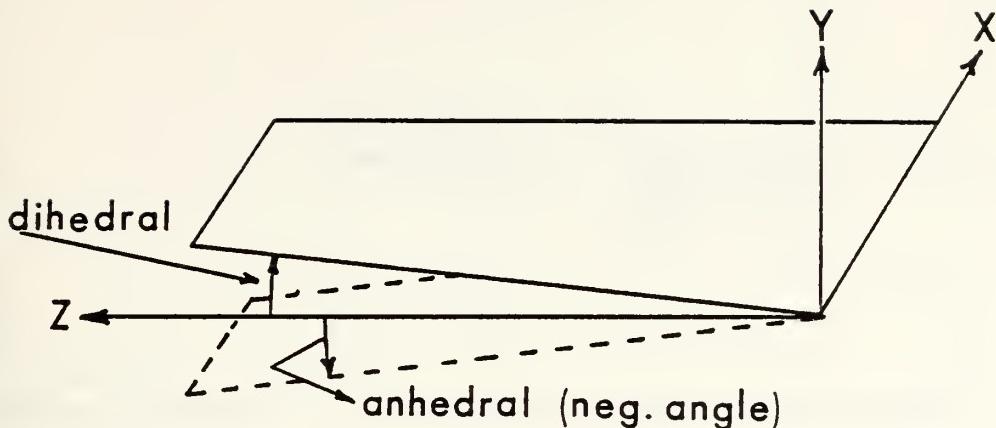


Figure 2.1. Dihedral Angle

Data input cards from 10 through 15 are used for defining wing planforms and section geometrics. For the first wing section, all data cards from card 10 through card 15 must be used. For the second and subsequent sections there is an option for skipping the wing section defining data (cards 12 through 15) and copying the data from that of the previous section. This option is controlled by the input variable FSEC. If this option is not used, data cards from 10 through 15 must be repeated for each wing defining section. The number of wing sections which are defined is input with the variable FNS. Remember, up to 11 sections may be defined, and a minimum of 3 sections must be defined. All wing planform and section defining geometrics must be in consistent units. Wing planform and section defining quantities are presented in Fig. 2.2.

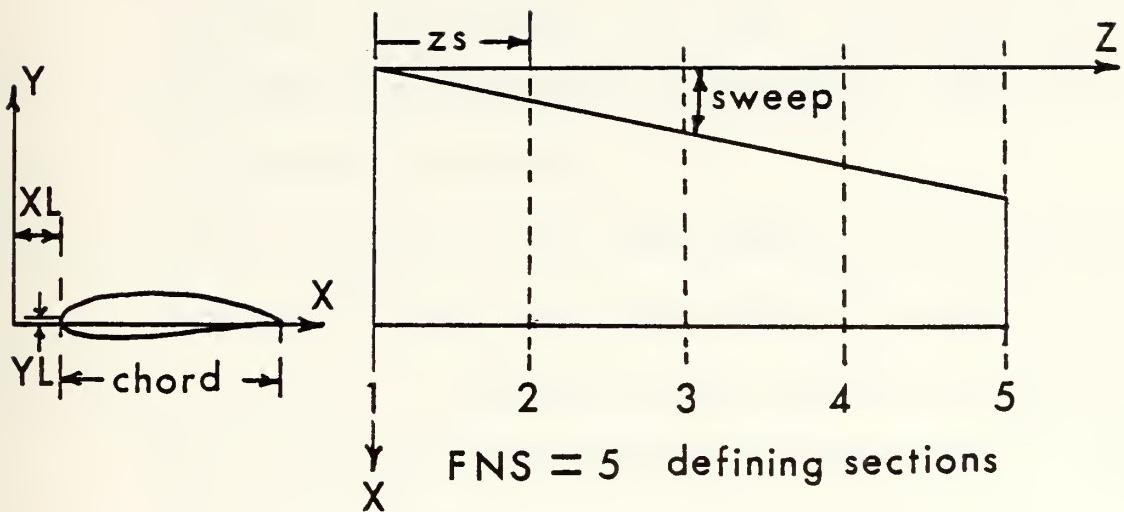


Figure 2.2. Wing Defining Geometry

CARD 10 Title card for the input variables

ZS, XI, YL, CHORD, THICK, AT and FSEC

CARD 11

Cols. 1-10 ZS - The section spanwise coordinate

(Start at the centerline and work
outboard)

Cols. 11-20 XL - Section leading edge X coordinate

Cols. 21-30 YL - Section leading edge Y coordinate

Cols. 31-40 CHORD - Section chord length

Cols. 41-50 THICK - The thickness scaling factor can be used to scale all Y coordinates of the wing section. Thus percent thickness and camber are increased (or decreased) accordingly. Use 1.0 if no scaling is desired.

Cols. 51-60 AT - The twist angle of each section (geometric twist) measured from the X axis to the chord line. A positive twist angle reduces the section angle of attack and gives "washout". Use 0.0 for no twist.

Cols. 61-70 FSEC - This is a flag which determines whether or not the program reads wing section defining geometry from a previous wing section or from new defining geometry. For the first section defined you must set FSEC to 1.0. Following the first section, if you define new section geometry then use FSEC = 1.0. If you want the program to read the section geometry defined from the previous section then set FSEC = 0.0.

CARD 12 Title card for the input variable

FN

CARD 13

Ccls. 1-10 FN - This variable contains the number of points which define the upper and lower surface of the section. A maximum of 161 points may be used.

CARD 14 Title card for the input variables

XP(I) and YP(I)

CARDS 15-1 to 15-N Total number of cards equals N,

where N = integer part of $(FN+2)/3$.

The X and Y coordinates at each point are entered in pairs, three points to a card. (See Appendix C for sample input)

Ccls. 1-10 XP(I) - X coordinate of the wing
section point

11-20 YP(I) - Y coordinate of the wing
section point

21-30 defining X coordinate for next
point

31-40 defining Y coordinate for next
point

41-50 defining X coordinate for
following point

The X and Y coordinates of the wing section defining points must be entered starting with the upper surface trailing edge point and proceeding along the upper surface to the leading edge, and returning along the lower surface to the lower surface trailing edge point. It is very important to define the section leading edge with a large number of closely spaced points. Suggest at least 0.05 spacing or less between X coordinate values from 0.1 X/C to the leading edge, $X/C = 0.0$. Each X and Y coordinate point is normalized using the chord length for that section. Section defining geometrics are illustrated in Fig. 2.3.

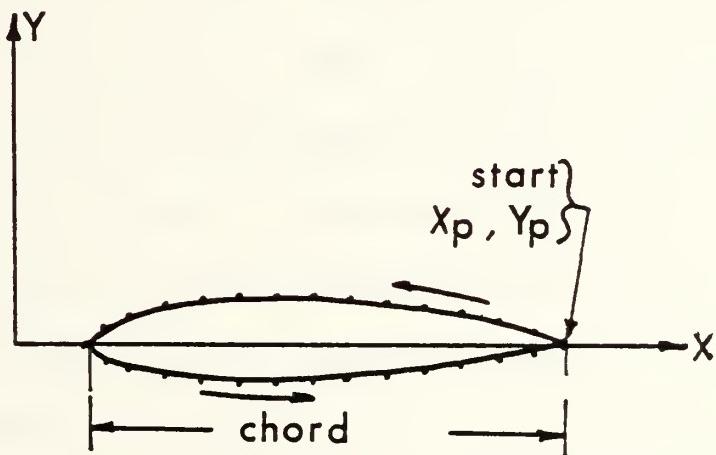


Figure 2.3. Section Defining Geometry

CARD 16 Title card containing the words in Cols. 1-80

END OF CALCULATIONS

CARD 17 Title card for the input variable

FNX

CARD 18

Cols. 1-10 FNX - This variable indicates the end of a set of calculations and must be set equal to 0.0. Its purpose is to indicate that the program has run to completion.

2. Program Output

Output from the FLC27 program varies with the value of the input variable FPLCT. When FPLOT is set equal to 0.0 a normal output is produced. This normal output contains (in order of occurrence): refined input geometry data including trailing edge slope and angle calculations; iterative solution of the potential flow mesh; section characteristics and wing characteristics. The iterative solution, section and wing characteristic data are repeated for each mesh refinement requested. Thus, if the input variable FMESH is set equal to 3, these data are calculated and output three times. The last data in the normal output consists of the non-dimensionalized chord (X/C) and pressure

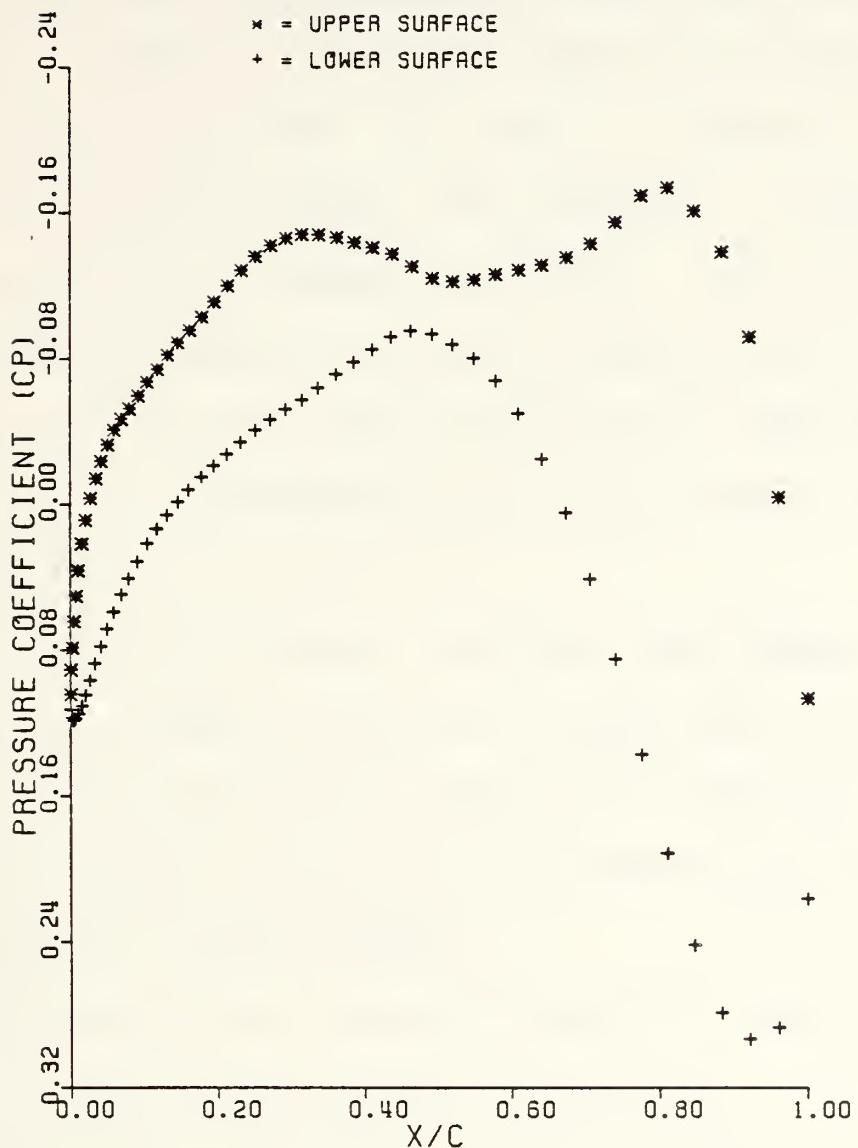
coefficient (C_p) data at each computational mesh point for each wing section calculated during the final mesh. A sample of the normal output data is presented in Appendix D and represents the output data from Appendix C input data.

If variable FPLOT is set equal to 1.0, the output data is increased considerably. This output contains the normal output plus a line printer-plot of the pressure coefficient at each computational mesh point for each wing section. The line printer-plot is produced for each wing section of each mesh refinement. The length of the output data with FPLOT set equal to 1.0 can approach 6000 records depending on the number of mesh refinements requested. These plots are of questionable value and, therefore, an alternate plotting program was developed.

When the variable FPLOT is set equal to 2.0, the normal output data is produced plus a Versatec plotting subroutine (VERTEC) is called. The subroutine outputs, via the Versatec plotter, plots of C_p versus X/C for each wing section of the final mesh calculations. This routine is simply putting into plot form the C_p and X/C numerical data contained in the normal output. A sample of the Versatec plot is presented in Fig. 2.4.

SECTION CP DATA

* = UPPER SURFACE
 + = LOWER SURFACE



SPAN STATION = 2.550

MACH 0.800

CL 0.34675

TAW 0.000

CD 0.02234

AOA 2.000

CM 0.00123

Figure 2.4. Versatec Plot of Cp vs. X/C

III. INTERACTIVE INPUT PROGRAM FLO27IN

The input data file required for the FLO27 program is extensive. Errors in input data FORMAT will cause program errors at execution time. In order to eliminate these errors and reduce the input data workload, a computer terminal interactive program was written. This interactive program, called FLO27IN, is a user-friendly way of creating an input data file for the potential flow wing analysis program FLO27. The FLO27IN program source code is presented in Appendix F.

The interactive program, FLO27IN, when executed ask's questions of the user in order to construct and write to the user's "A" disk the required FLO27 input data file. The following presents the step-by-step procedure for executing the interactive program FLO27IN.

STEP #1---Log on to any IBM 3033 interactive terminal
with your user number and password.

STEP #2---Once logged on and in the CMS operation mode
type:

CP LINK 0247P 191 120 RR then hit ENTER

STEP #3---The word PASSWORD will appear, Type and ENTER
AERO

STEP #4---Type and ENTER

ACC 120 D

STEP #5---Type and ENTER

LOAD FLO27IN (START

The screen will display the header for the interactive program. Answer each question presented. At the end of each question in parenthesis is the input data variable associated with that question and whether the input parameter is a real number (R) or an integer (I). Example:
==> Enter the free stream Mach number (FMACH): (R). FMACH is the input data variable for the question. As you proceed through the FLC27IN program, opportunities to review and change input data will be presented. Should it become necessary to change your input data after completing the FLO27IN program, you can simply XEDIT the created data file.

The FLO27IN program also incorporates a library which contains the wing-section defining data for a number of current wing shapes. A copy of this library is presented in Appendix B. This feature will be displayed during program execution by the use of a menu from which the user can select a pre-defined wing section or define his own.

Upon completion of user inputs to the interactive program three additional data lines are automatically written to the bottom of the input file. They are:

END OF CALCULATION

FN X

0.0

In addition, Job Control Language (JCL) cards are written to the top and bottom of the file. All JCL cards start with a // format. After FL027IN has run to completion type and enter RELEASE 191 to release the aero disk which was linked while executing the FL027IN program. The created data file is written to the user's "A" disk with <filename> <filetype> of FL027 DATAIN. Additional changes can be made simply by entering the XEDIT mode and editing the file.

IV. FLO27 BATCH SYSTEM EXECUTION

The potential flow program FLO27 can be executed after the input data file has been created. The batch processor is required for FLO27 execution because of the extensive CPU time needed to run the program. While in the XEDIT mode, a standard JCB card must be added to the top of the FLO27 DATAIN file prior to submission for job execution. The JOB card has the form:

```
//jobname JOB (nnnn,pppp),'ident',CLASS=J
```

jobname = may contain up to 8 alphanumeric characters,
the first of which must be alphabetic.

nnnn = your user number

pppp = project number, assigned by professor

'ident' = contains the user's own identification
information. A maximum of 20 characters may be
contained within the single quotation marks.

After adding the JOB card to your data file, you are ready to execute the program. Type SUBMIT FLO27 DATAIN and press ENTER. Batch runs are normally not worth waiting for. To inquire about the status of the job, enter INQ and the job name used on the JOB card or "logoff". If the system is busy and the maximum mesh size was selected, it may be several hours before your job is run.

When the job is run the output will be spooled to the batch printer located next to the VM printer in the main computer building. The title at the top of the printout for batch jobs is the name entered on the JOB card. If it is desired to have the program output data spooled directly to the terminal, it will be necessary to add one additional JCL card to the input data set. This card must be placed immediately following the JOB card and has the form:

```
//*MAIN ORG=NPGVM1.nnnnP
```

where nnnn = your user number

Inserting this card in the input data will cause all program output to be spooled to the user's virtual reader where it may be looked at, printed or transferred to his "A" disk. To enquire as to whether information is in the reader simply type RDR and hit enter, then follow the instructions on the screen.

V. PROGRAM TEST RESULTS

The FLO27 program was tested in three stages; (1) during the reprogramming phase for conversion completeness, (2) after successful conversion with suitable wing data for program accuracy and (3) during an AE-4501 class project.

A. ACCEPTANCE TEST DATA

To test and ensure that the FLO27 program was converted to IBM compatible Fortran without error, an acceptance test data set was used. The acceptance test input and output data was supplied with the original CDC program source code. After conversion of the FLO27 program to Fortran suitable for the NPS IBM system, the acceptance test input data were run and the output results compared to the output generated by the CDC system.

Both output data sets were numerically exact when the FLO27 program was run in double precision on the IBM system. If the program was run in single precision, the numerical output values were exact to the third decimal place. The difference in single precision accuracy occurs because the CDC system uses a 64 bit word length while the IBM system word length in single precision is only 32 bits. It was

decided that the IBM single precision accuracy was satisfactory.

B. COMPARISON WITH OTHER PROGRAMS

The FLC27 program was also tested for accuracy by using the wing planform and section data from a NACA 572 wing. The data were run on both the FLO27 program and the Douglas potential flow program [Ref. 1]. The data generated by both programs was compared to wind tunnel data for the NACA 572 wing [Ref. 8]. The results are presented in Fig. 5.1 as plots of lift coefficient versus angle-of-attack. The results show that for the NACA 572 wing the FLO27 program more accurately predicts the wing lift coefficient than does the Douglas program.

C. AE-4501 CLASS PROJECT

The final test phase was conducted by introducing the FLO27 program into the AE-4501 course as a class project. This was accomplished to determine student problems/comments concerning the data input program FLO27IN and to test an additional wing shape. The wing chosen for study was that of the A-7 airplane. The A-7 wing has a distinct leading edge notch at the approximate mid-span. When the planform geometry was run with the notch included the FLO27 program

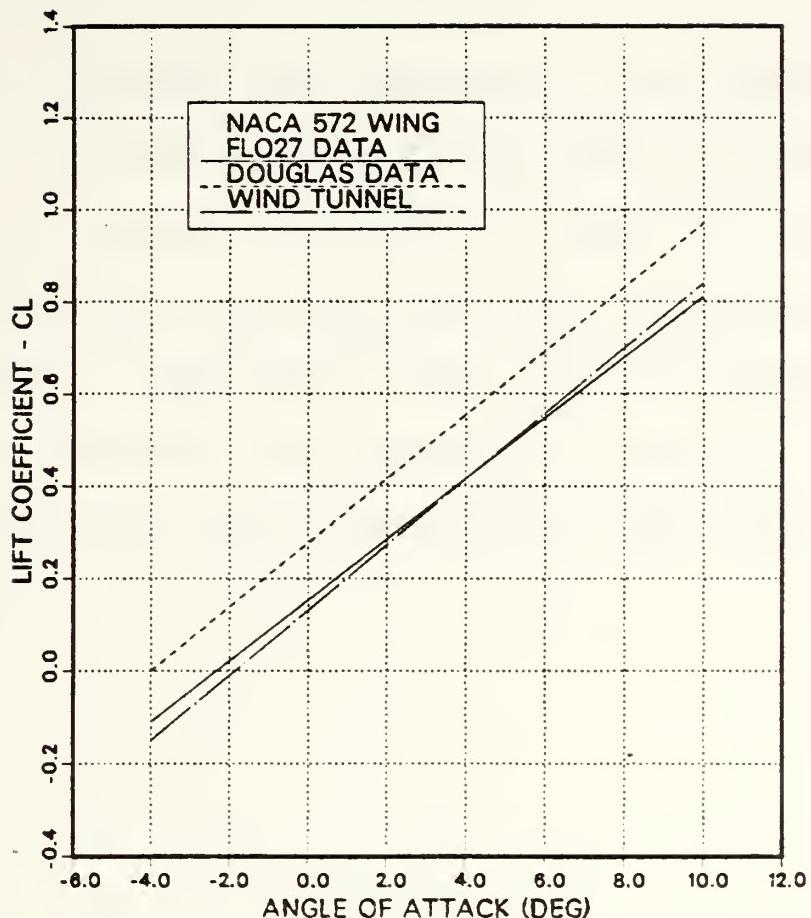


Figure 5.1. Program Calculated and Wind Tunnel Data

ran to completion but gave negative values for section and total induced drag coefficient. The value for the lift coefficient was low for the freestream Mach and angle-of-attack used. It was found that if the notch was

excluded from the wing geometry input data the program results were satisfactory both for induced drag and lift coefficient.

From the AE-4501 class experience it was determined that sharp wing planform discontinuities cannot be handled by the program. If however, the changes in shape are gradual, such as a wing glove, the program output appears to be satisfactory. Such was the case with the acceptance test case data where the wing geometry was that of the F-8 supercritical wing which incorporates a wing glove.

APPENDIX A

C This JCL routine allocates sufficient space on the mass
C storage system to store the entire tape contents
//JACK JOB (3266,0178),'PASCHALL-2759',CLASS=A
///*MAIN ORG=NPGVM1.3266P
// EXEC PGM=IEFBR14
//DD1 DD UNIT=3330V,MSVGP=PUB4C,DISP=(NEW,CATLG),
// DSN=MSS.S3266.WFLOW.DATA,SPACE=(CYL,(16,4,2))
/*
//

C This JCL routine is used to transfer all tape files to
C a partitioned data set in the mass storage system
//JACK JOB (3266,0178),'PASCHALL-2759',CLASS=J
///*MAIN ORG=NPGVM1.3266P
//COPY PROC FILE=,MEM=
// EXEC PGM=IEBGENER
//SYSPRINT DD SYSOUT=A
//SYSIN DD DUMMY
//SYSUT1 DD UNIT=3400-6,VOL=SER=WFLOW,DISP=(OLD,PASS),
// LABEL=(FILE,BLP,IN)
// DCB=(RECFM=F,BLKSIZE=80,DEN=3,OPTCD=Q)
//SYSUT2 DD DISP=(OLD,KEEP),
// DSN=MSS.S3266.WFLOW.SOURCE(&MEM)
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=6400)
// PEND
// EXEC COPY,FILE=1,MEM=FLO27
// EXEC COPY,FILE=2,MEM=A411IN
// EXEC COPY,FILE=3,MEM=VWIN
// EXEC COPY,FILE=4,MEM=A411AO1
// EXEC COPY,FILE=5,MEM=INTERF
// EXEC COPY,FILE=6,MEM=A411PS
// EXEC COPY,FILE=7,MEM=A411P1
// EXEC COPY,FILE=8,MEM=A411P2
// EXEC COPY,FILE=9,MEM=COUPLE
// EXEC COPY,FILE=10,MEM=ITER
// EXEC COPY,FILE=11,MEM=DATAIN
// EXEC COPY,FILE=12,MEM=FINAL
// EXEC COPY,FILE=13,MEM=BOEB1
// EXEC COPY,FILE=14,MEM=CONTPLT
// EXEC COPY,FILE=15,MEM=CORDPLT
// EXEC COPY,FILE=16,MEM=STREPLT
//COPY2 PROC FILE=,MEM=,LRECL=80,BLK=6400
// EXEC PGM=IEBGENER
//SYSPRINT DD SYSOUT=A
//SYSIN DD DUMMY
//SYSUT1 DD UNIT=3400-6,VOL=SER=WFLOW,DISP=(OLD,PASS),
// LABEL=(FILE,BLP,IN)
// DCB=(RECFM=F,BLKSIZE=&LRECL,DEN=3,OPTCD=Q)
//SYSUT2 DD DISP=(OLD,KEEP),DSN=MSS.S3266.WFLOW.DATA(&MEM),
// DCB=(RECFM=FB,LRECL=&LRECL,BLKSIZE=&BLK)
// PEND
// EXEC COPY2,FILE=17,LRECL=150,BLK=6000,MEM=OUTF27
// EXEC COPY2,FILE=18,LRECL=150,BLK=6000,MEM=OUTIFC
// EXEC COPY2,FILE=19,LRECL=150,BLK=6000,MEM=OUT411L
// EXEC COPY2,FILE=20,LRECL=150,BLK=6000,MEM=OUT411U
/*
//

C This JCL routine moves all source code files from mass
C storage to the MVS 004 disk which can be accessed by
C entering GET MVS then following the screen instructions
C to move source files to your disk. If you want to move
C the data files to MVS 004 then change the word SOURCE
C to DATA in the JCL program below.

```
//JACK JOB (3266,0178), 'FASCHALL-2759', CLASS=A
//**MAIN ORG=NPGVM1.3266P
// EXEC PGM=IEBCOPY
//SYSPRINT DD SYSOUT=A
//FROM DD DISP=SHR,DSN=MSS.S3266.WFLOW.SOURCE
//INTO DD UNIT=3350,VOL=SER=MVS004,DISP=(NEW,KEEP),
//      SPACE=(CYL,(16,4,10),RLSE),DSN=S3266.SOURCE
//SYSUT3 DD UNIT=SYSDA,SPACE=(CYL,(2,2))
//SYSUT4 DD UNIT=SYSDA,SPACE=(CYL,(2,2))
//SYSIN DD *
   COPY OUTDD=INTC,INDD=FFCM
/*
//
```


APPENDIX B

LITERARY OF AIRFOIL SECTION GEOMETRIES

- 0 = user input section coordinate data
- 1 = flat plate data
- 2 = symmetrical wing (11% thickness at 30% chord)
- 3 = supercritical wing (cambered, 12% thickness at 32% chord)
- 4 = NACA 24-30-0 (cambered, 12% thickness at 30% chord)
- 5 = F-14 wing (cambered, 9.5% thickness at 37% chord)
- 6 = A-7 wing (7 deg droop at 20% chord, 7% thickness at 43% chord)
- 7 = LISSAMAN 7769 Airfoil (cambered, 11% thickness at 30% chord)
- 8 = NACA 0010 (symmetrical, 10% thickness at 30% chord)
- 9 = NACA 0010-34 (symmetrical, 10% thickness at 40% chord)
- 10 = NACA 0010-35 (symmetrical, 10% thickness at 50% chord)
- 11 = NACA 0010-64 (symmetrical, 10% thickness at 40% chord)
- 12 = NACA 0010-66 (symmetrical, 10% thickness at 60% chord)
- 13 = NACA 16-009 (symmetrical, 9% thickness at 50% chord)
- 14 = NACA 63-010 (symmetrical, 10% thickness at 35% chord)
- 15 = NACA 63A010 (symmetrical, 10% thickness at 35% chord)
- 16 = NACA 64-010 (symmetrical, 10% thickness at 40% chord)
- 17 = NACA 64A010 (symmetrical, 10% thickness at 40% chord)
- 18 = NACA 65-010 (symmetrical, 10% thickness at 40% chord)
- 19 = NACA 65A010 (symmetrical, 10% thickness at 40% chord)
- 20 = NACA 66-010 (symmetrical, 10% thickness at 45% chord)

APPENDIX C

THIS APPENDIX PRESENTS A COMPLETE INPUT DATA SET INCLUDING THE JCL CARDS REQUIRED TO EXECUTE THE PROGRAM FLC27

```

// ( STANDARD JOB CARD - SEE MVS USER'S GUIDE NO. RV5-01)
// EXEC FLC27
// GO SYSIN DD *  

// SAM FILE DATA (NACA 572 WING SECTION)
// FNX FNY F12 FMESH FFLOT 0.0
40.0 4.0 P10 3.0
FIT 0.0001 1.0
100.0 0.0001 1.0
20.0 0.0001 1.0
5.0 0.0001 1.0
FMACF 0.10 0.0001 1.0
ZSYM 1.0 0.0001 1.0
ZS 0.0 0.0001 1.0
FN 41.0 C YP (I) YP (I)
X1.0 0.0000 0.0013000 C.950000 0.0120000 C.900000 0.0204000
0.005000 0.0013000 C.076000 0.00515000 0.600000 0.0642000
0.025000 0.0013000 C.073000 0.00780000 0.300000 0.0788000
0.01030000 0.0013000 C.07680000 0.00726000 0.150000 0.0661000
0.005000 0.0013000 C.05630000 0.00414000 0.040000 0.0350000
0.00250000 0.0013000 C.02500000 0.00220000 0.010000 0.0128000
0.00050000 0.0013000 C.00500000 0.00050000 0.001000 0.000000
0.00025000 0.0013000 C.00500000 0.00025000 0.0001000 0.000000
0.0001020000 0.0013000 C.01680000 0.00030000 0.000227000 0.0120000
0.0002050000 0.0013000 C.03020000 0.00100000 0.000375000 0.0268000
0.00020000 0.0013000 C.04220000 0.00250000 0.000422000 0.0420000
0.00040000 0.0013000 C.03580000 0.00250000 0.000320000 0.0412000
0.00070000 0.0013000 C.02150000 0.00350000 0.000320000 0.0260000
0.00095000 0.0013000 C.0048000 0.00013000 0.000150000 0.0082000
ZS 6875 XL YL CHRD THICK AT FSEC
ZS 9. 6875 XL 6.1307 YL 0. C 6.4500 CHRD THICK AT 0.0 OSEC
ZS 19. 3750 XL 12.2614 0.0 4.3000 THICK 1.00000 0.0 FSEC
FNX 0.0 /* //
```


APPENDIX D

THIS APPENDIX PRESENTS THE FLC27 OUTPUT DATA PRODUCED FROM THE INPUT DATA OF THE PREVIOUS APPENDIX.

A46C MODIFIED FROM FLC27 OF ANTENNA JAMESON CURRENT INSTANTANEOUS IN TRANSONIC FLOW USING FINITE VOLUME SCHEME
 THREE DIMENSIONAL WING ANALYSIS IN NACA 572 WING SECTION
 FUSELAGE RAE

0.0 SWEEP SWEEP
 32.3275 0.0

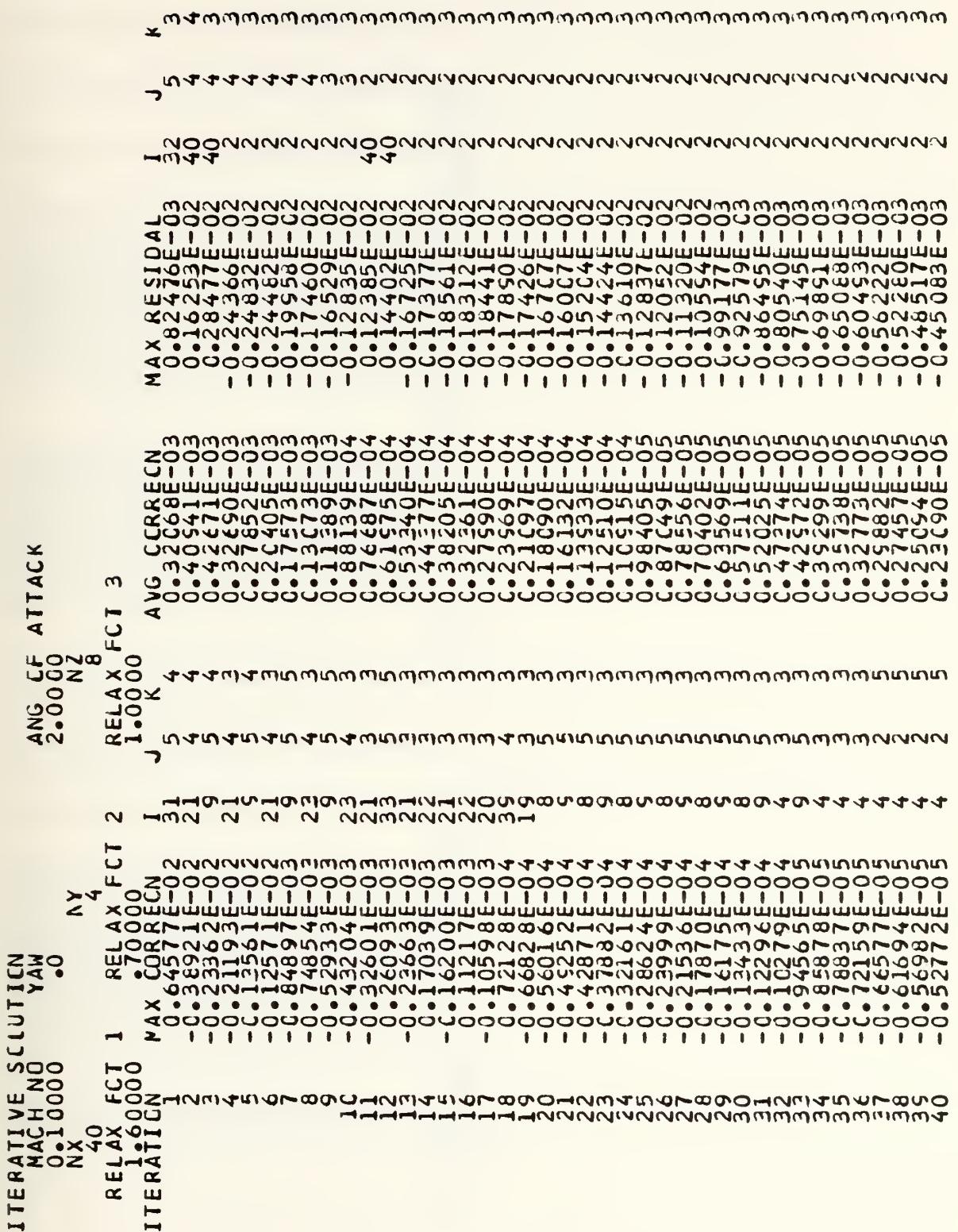
PROFILE AT $\frac{Z}{R}$ = 0.1 C SLOPE
 16.0833 -0.0720

NL = 21, XF(NL) = 0.0
 (XP, YP)

NL = 21, XF(NL) = 0.0

(XP, YP)

1.00000	-0.00130	0.95000	-0.00480	0.90000	-0.00820
0.60000	-0.02600	0.50000	-0.03200	0.40000	-0.03580
0.20000	-0.04220	0.15000	-0.04200	0.10000	-0.03750
0.03000	-0.02270	0.02000	-0.01680	0.01000	-0.01200
0.0	0.0	0.0250	0.01500	0.0500	0.04700
0.03000	0.02900	0.04000	0.03500	0.05000	0.04140
0.02000	0.07260	0.25000	0.07680	0.30000	0.07880
0.06000	0.06420	0.70000	0.05150	0.80000	0.03760
1.00000	0.00130	0.0	0.0	CHORD 8.6000	TWIST 0.0
0.0	0.0	JMIN YMAX	7.880E-01	JMAX 33	YDF 1210
SECTION LE DEFINITION AT Z = 10	YLE	9.6875	CHORD 6.4500	THICKNESS RATIO 1.0000	TWIST 0.0
SECTION LE DEFINITION AT Z = 10	YLE	0.0	YMAX	JMAX 33	YDF 1210
SECTION LE DEFINITION AT Z = 10	YLE	0.0	7.880E-01	CHORD 4.3000	THICKNESS RATIO 1.0000
SECTION LE DEFINITION AT Z = 10	YLE	0.0	YMAX	JMAX 33	YDF 1210
SECTION LE DEFINITION AT Z = 10	YLE	0.0	7.880E-01	CHORD 4.3000	THICKNESS RATIO 1.0000
SECTION LE DEFINITION AT Z = 10	YLE	0.0	YMAX	JMAX 33	YDF 1210



SECTION CHARACTERISTICS

MACH NO	YAW	ANG CF	ATTACK
0.10000	-0	CL	2.0000
0.0	•20238	CD	CM
3•87499	•24033	•71088E-02	•91575E-01
7•74599	•26515	•24623E-C2	•96798E-01
11•62498	•28127	•48115E-02	•1C506
15•49998	•28695	•57074E-02	•1C920
19•37497	•24168	•65491E-C2	•1C935
		•70588E-02	•86038E-01

WING CHARACTERISTICS

MACH NO	YAW	ANG CF	ATTACK
0.10000	•0	CD	2.0000
0.25575	-•32534E-02	•10000E-01	CD
CM YAW	•23919	•7466E-02	FRIC TION
-0.00467		-•33140	CM PITCH

ANG CF

ATTACK	CD	CM	L/D FORM	V D
2.0000	•67466E-02	-78.612		•7.
CL	•33140			
FRIC TION				
CM PITCH				

ITERATIVE SOLUTION
MACH NO YAW
0.10000 .0
ANG CF ATTACK
2.0000

SECTION CHARACTERISTICS

MACH NO	YAW	ANG CF ATTACK
0.1000	0	2.0000
SPAN STATION	CL	• 18197E-01
0.0		• 53303E-02
1.93750	• 22093	• 14194E-C2
3.87499	• 24319	• 44517E-C5
5.81249	• 26091	• 72064E-03
7.74996	• 27508	• 11994E-C2
9.68749	• 28683	• 16262E-02
11.62499	• 29643	• 20637E-02
13.56248	• 30359	• 27385E-C2
15.59998	• 30863	• 41059E-02
17.43746	• 30746	• 42003E-C2
19.37497	• 29141	
	• 21866	
	-0.78297E-01	

WING CHARACTERISTICS

MACH NO	YAW	ANG CF ATTACK
0.1000	0	2.0000
CL	CD FORM	CD FRICTION
0.27663	• 87151E-03	• 10000E-01
CW YAW	CW ROLL	CW PITCH
-0.00145	.25615	-0.35963

ANG CF ATTACK

SPAN STATION	CL	CM	L/D FORM	L/D
0.0			• 1C872E-01	25.
1.93750	• 22093	• 18197E-01		
3.87499	• 24319	• 53303E-02		
5.81249	• 26091	• 14194E-C2		
7.74996	• 27508	• 44517E-C5		
9.68749	• 28683	• 72064E-03		
11.62499	• 29643	• 11994E-C2		
13.56248	• 30359	• 16262E-02		
15.59998	• 30863	• 20637E-02		
17.43746	• 30746	• 27385E-C2		
19.37497	• 29141	• 41059E-02		
	• 21866	• 42003E-C2		
	-0.78297E-01			

ITERATIVE SCLUTION	MACH NO	YAW	ANG OF ATTACK
ITERATION	0.1	0.0	2.0000
ITERATION	0.1	0.0	2.0000
ITERATION	0.1	0.0	2.0000
MAX RESIDAL	-0.1385	E-C2	0.6224E-03

K-24
 23 3 23
 AVG CORREC N MAX RESIDAL I J
 C-2 0565E-04 -0.13855E-02 1 2 16
 C-1 2764E-04 0.99673E-03 160 15
 C-0 96247E-05 0.87373E-03 160 15
 C-0 79284E-05 0.73407E-03 160 15
 C-0.7 1493E-05 0.62249E-03 160 15
 WORK RELUCTN/CYCLE CONV TOLERENCE
 4.000C 0.8187 0.1000E-05

SECTION CHARACTERISTICS

ANG OF ATTACK

MACH NO	YAW	CL	CD	CM
0.0	0.0	2.536	2.22E-01	1.0517
0.1	0.0	2.3679	3.4E-01	1.0917
0.2	0.0	2.25693	5.3E-01	1.1244
0.3	0.0	2.2726	5.9E-01	1.1393
0.4	0.0	2.27957	6.5E-01	1.1684
0.5	0.0	2.28124	7.0E-01	1.1821
0.6	0.0	2.28459	7.5E-01	1.1944
0.7	0.0	2.29155	8.0E-01	1.2056
0.8	0.0	2.29463	8.5E-01	1.2147
0.9	0.0	2.29631	9.0E-01	1.2249
1.0	0.0	2.30116	9.5E-01	1.2276
1.1	0.0	2.30527	1.0E-01	1.2287
1.2	0.0	2.30877	1.05E-01	1.235
1.3	0.0	2.31151	1.1E-01	1.2093
1.4	0.0	2.31326	1.15E-01	1.1776
1.5	0.0	2.31355	1.2E-01	1.177
1.6	0.0	2.31168	1.25E-01	1.299E-01
1.7	0.0	2.30595	1.3E-01	1.38273E-01
1.8	0.0	2.29369	1.35E-01	1.469591E-01
1.9	0.0	2.26619	1.4E-01	1.549591E-01
2.0	0.0	2.20055	1.45E-01	1.68299E-01

WING CHARACTERISTICS

MACH NO	YAW	ANG OF ATTACK	CD	CM	L/D FORM
0.0	0.0	2.0000	0.0000	1.3832E-01	73.379
0.1	CL	CD FCRM	1.00CDE-01	1.3832E-01	73.379
0.2	8117	3.8318E-02	CW PITCH	-	73.379
CM YAW	CM ROLL	0.25975	-0.36670		
0.00116					

A46C MODIFIED FROM FLC27 OF ANTONY JAMESON CURRENT INST ILUTE THREE-DIMENSIONAL WING ANALYSIS IN TRANSonic FLOW USING FINITE VOLUME SCHEME PREPARED BY DR. HAI-CHOW CHEN STANDARD BOEING VERSION 1.0 OF CALCULATION

$$\text{SPAN STATION} = \frac{\text{CF DATA POINTS}}{\text{NO.}} = \frac{1.93}{101} 750$$

CF 588
 246788020801542388213722474-37
 1000001212112583030544444732001
 00000000000000000000000000000000
 - - - - - - - - - - - - - - - - - - -
 X/C 857
 3890694513683581346963718483969
 88401077313581346963718483969
 88401077313581346963718483969
 88401077313581346963718483969
 00000000000000000000000000000000
 - - - - - - - - - - - - - - - - - - -
 CP 4833014569715412574125639469404
 585343380145697154125639469404
 585343380145697154125639469404
 585343380145697154125639469404
 00000000000000000000000000000000
 - - - - - - - - - - - - - - - - - - -
 CP 62648330145697154125639469404
 585343380145697154125639469404
 585343380145697154125639469404
 585343380145697154125639469404
 00000000000000000000000000000000
 - - - - - - - - - - - - - - - - - - -
 X/C 774156415641564156415641564156
 7741564156415641564156415641564156
 7741564156415641564156415641564156
 7741564156415641564156415641564156
 00000000000000000000000000000000000000
 - - - - - - - - - - - - - - - - - - -
 CP 13C84696665154344467284164441074
 124696665154344467284164441074
 124696665154344467284164441074
 124696665154344467284164441074
 00000000000000000000000000000000000000
 - - - - - - - - - - - - - - - - - - -
 CP 13C84696665154344467284164441074
 124696665154344467284164441074
 124696665154344467284164441074
 124696665154344467284164441074
 00000000000000000000000000000000000000
 - - - - - - - - - - - - - - - - - - -

SPAN NO.	STATION CF	DATA POINTS	Σ	90' 25"
	X/C	CP	X/C	
1.	C00 000	C. 236239	0. 56	
	0. 846 730	C. 102997	0. 81	
	0. 706 152	C. C29155	0. 67	

0.207084	$\frac{CP}{X/C}$	0.921777	0.161171
0.080654	$\frac{CP}{X/C}$	0.774854	0.059673
0.025745	$\frac{CP}{X/C}$	0.640641	0.027657

SPAN STATION NO. OF DATA POINTS = 7074959 / 101

SPAN STATION = PGINTS = 5.68749
 NO. OF DATA X/C CP
 1 0.035734 -C 2464650
 2 0.072512 -C 6655513
 3 0.124444 -C 54093
 4 0.1889467 -C 660565
 5 0.23572655 -C 3224544
 6 0.2606692 -C 639055
 7 0.30551460 -C 339038
 8 0.35705038 -C 750080
 9 0.40351519 -C 519890
 10 0.0000000001 -C 0.0000000000

SPAN STATION = PGINTS = 101
 NO. OF DATA X/C CP
 1 0.03573492 -C 0.03960492
 2 0.08461527 -C 0.04617092
 3 0.13086924 -C 0.05860560
 4 0.18028692 -C 0.08412419
 5 0.23087192 -C 0.11692419
 6 0.28023412 -C 0.14686924
 7 0.33024124 -C 0.17670560
 8 0.38024124 -C 0.20667467
 9 0.43024124 -C 0.23666967
 10 0.48024124 -C 0.28666967
 11 0.53024124 -C 0.33666967
 12 0.58024124 -C 0.38666967
 13 0.63024124 -C 0.43666967
 14 0.68024124 -C 0.48666967
 15 0.73024124 -C 0.53666967
 16 0.78024124 -C 0.58666967
 17 0.83024124 -C 0.63666967
 18 0.88024124 -C 0.68666967
 19 0.93024124 -C 0.73666967
 20 0.98024124 -C 0.78666967
 21 1.03024124 -C 0.83666967
 22 1.08024124 -C 0.88666967
 23 1.13024124 -C 0.93666967
 24 1.18024124 -C 0.98666967
 25 1.23024124 -C 1.03666967
 26 1.28024124 -C 1.08666967
 27 1.33024124 -C 1.13666967
 28 1.38024124 -C 1.18666967
 29 1.43024124 -C 1.23666967
 30 1.48024124 -C 1.28666967
 31 1.53024124 -C 1.33666967
 32 1.58024124 -C 1.38666967
 33 1.63024124 -C 1.43666967
 34 1.68024124 -C 1.48666967
 35 1.73024124 -C 1.53666967
 36 1.78024124 -C 1.58666967
 37 1.83024124 -C 1.63666967
 38 1.88024124 -C 1.68666967
 39 1.93024124 -C 1.73666967
 40 1.98024124 -C 1.78666967
 41 2.03024124 -C 1.83666967
 42 2.08024124 -C 1.88666967
 43 2.13024124 -C 1.93666967
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 51 2.53024124 -C 2.33666967
 52 2.58024124 -C 2.38666967
 53 2.63024124 -C 2.43666967
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 56 2.78024124 -C 2.58666967
 57 2.83024124 -C 2.63666967
 58 2.88024124 -C 2.68666967
 59 2.93024124 -C 2.73666967
 60 2.98024124 -C 2.78666967
 61 3.03024124 -C 2.83666967
 62 3.08024124 -C 2.88666967
 63 3.13024124 -C 2.93666967
 64 3.18024124 -C 2.98666967
 65 3.23024124 -C 3.03666967
 66 3.28024124 -C 3.08666967
 67 3.33024124 -C 3.13666967
 68 3.38024124 -C 3.18666967
 69 3.43024124 -C 3.23666967
 70 3.48024124 -C 3.28666967
 71 3.53024124 -C 3.33666967
 72 3.58024124 -C 3.38666967
 73 3.63024124 -C 3.43666967
 74 3.68024124 -C 3.48666967
 75 3.73024124 -C 3.53666967
 76 3.78024124 -C 3.58666967
 77 3.83024124 -C 3.63666967
 78 3.88024124 -C 3.68666967
 79 3.93024124 -C 3.73666967
 80 3.98024124 -C 3.78666967
 81 4.03024124 -C 3.83666967
 82 4.08024124 -C 3.88666967
 83 4.13024124 -C 3.93666967
 84 4.18024124 -C 3.98666967
 85 4.23024124 -C 4.03666967
 86 4.28024124 -C 4.08666967
 87 4.33024124 -C 4.13666967
 88 4.38024124 -C 4.18666967
 89 4.43024124 -C 4.23666967
 90 4.48024124 -C 4.28666967
 91 4.53024124 -C 4.33666967
 92 4.58024124 -C 4.38666967
 93 4.63024124 -C 4.43666967
 94 4.68024124 -C 4.48666967
 95 4.73024124 -C 4.53666967
 96 4.78024124 -C 4.58666967
 97 4.83024124 -C 4.63666967
 98 4.88024124 -C 4.68666967
 99 4.93024124 -C 4.73666967
 100 4.98024124 -C 4.78666967
 101 5.03024124 -C 5.00000000

0 8 2 2 1 4 1 1 1 5 4 3 5 2 2 7 8 5 6
8 8 0 8 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
7 6 8 8 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
6 8 8 0 9 1 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
5 7 6 8 8 8 0 9 1 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
4 7 6 8 8 8 0 9 1 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
3 5 6 8 8 8 0 9 1 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
2 3 5 6 8 8 8 0 9 1 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
1 0 3 6 8 8 8 0 9 1 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
0 3 6 8 8 8 0 9 1 4 5 8 9 8 9 1 4 0 4 0 2 6 9 8
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581787280412467057195510
550785260414467057195510
603555757449567057195510
6801101257248867057195510
738001317248867057195510
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CP 6479601435805860279247303833
69300769601560002078861254270
1200000344141416346545454545
00000000000000000000000000000000

SPAN NO.	STATION NO.	CF	CA
1	000	000	000
2	000	07152	000
3	000	12980	000
4	000	05437	000
5	000	05235	000
6	000	05480	000
7	000	05078	000
8	000	05235	000
9	000	05480	000
10	000	05078	000
11	000	03703	000
12	000	03703	000
13	000	03703	000
14	000	03703	000
15	000	03703	000
16	000	03703	000
17	000	03703	000
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95	000	03703	000
96	000	03703	000
97	000	03703	000
98	000	03703	000
99	000	03703	000
100	000	03703	000

65

SPAN STATION = 15 • 49998
NO. OF DATA POINTS = 101

SPAN NO.	STATION	DATA POINTS	\bar{X}	C _P	X/C	C _P	X/C	C _P	X/C	C _P
1	X/1000000	C _P = 101	0.560494	0.195639	0.921779	0.149727	0.883859	0.11730	X/1000000	C _P = 101
2	0.846732	C _P = 224658	0.810358	0.072479	0.74855	0.052997	0.740107	0.05583	0.706153	C _P = 225340
3	0.706153	C _P = 293051	0.672999	0.023433	0.640643	0.026703	0.609078	0.02724		

0.460619	-0.245829	0.488450	-0.239440	0.517072	-0.229495	0.546466	-0.21668
0.576693	-0.204904	0.607655	-0.186239	0.639467	-0.163669	0.672057	-0.14166
0.705396	-0.124829	0.739503	-0.112534	0.774369	-0.097547	0.810060	-0.07234
0.846512	-0.036530	0.883731	-0.006437	0.924712	0.025749	0.960469	0.07570
1.000000	0.142642						

APPENDIX E

THIS APPENDIX PRESENTS THE SOURCE CODE FOR THE POTENTIAL FLOW PROGRAM FLO27.

***** FLC27*****9/12/83*****
 ***** THREE-DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING
 ***** FINITE VOLUME SCHEME WITH SHEARED PARABOLIC COORDINATES
 ***** PROGRAMMED BY ANTONY JAMESON, JANUARY-AFRIL 1977
 ***** THE BEING VERSION OF FLO27 WAS PREPARED BY ER. HAI-CHOW
 ***** CHEN WITH THE FOLLOWING MODIFICATIONS:
 1) TEMPORARY STORAGE OF THE LARGE CORE MEMORY REQUIREMENTS
 HAS BEEN IMPLEMENTED TO REDUCE THE COMPUTING COSTS
 BY BUFFERING DATA IN AND OUT OF CORE.
 2) STANDARD BOEING INPUT FORMAT FOR THE WING SECTION
 HAS BEEN USED.
 3) SUBPROGRAM BLIN HAS BEEN IMPLEMENTED TO ADD THE
 DISPLACEMENT THICKNESS TO THE ORIGINAL WING SECTIONS
 4) WING SECTION LEADING EDGE SINGULAR POINT IS FOUND BY
 COMPUTING THE FOCUS OF A PARABOLA BY LEAST-SQUARES FIT CENTERED AT THE LEADING EDGE POINT.
 THIS IS SUPPLIED BY THE USER THROUGH INPUT CARD.
 5) TRAILING EDGE CLOSURE ANGLE AND EISECKER SLOPE ARE
 COMPUTED BASED ON BACKWARD DIFFERENCE.
 6) CFTION FOR PRINTER-PLOTTING OF THE UNWRAPPED
 WING SECTIONS IS AVAILABLE

***** THE FOLLOWING FILES ARE USED TO EXECUTE FLO27. SOME OF THESE
 FILES ARE USED SUBSEQUENTLY IN OTHER MODULES OF THE VISCOUS/
 INVIScid INTERACTIVE WING SYSTEM
 FILE1 IS USED TO BUFFER DATA IN AND OUT OF CORE
 FILE2 IS USED TO BUFFER DATA IN AND OUT OF CORE
 FILE3 IS USED TO BUFFER DATA IN AND OUT OF CORE

FILE4 IS USED TO READ IN THE VELOCITY POTENTIAL
GENERATED PREVIOUSLY

FILE8 IS WRITTEN FOR DATA TRANSFER TO BEING
TURBULENT BOUNDARY LAYER PROGRAM A411.

FILE5 IS USED TO SAVE SECTION SURFACE PRESSURE
AGAINST X/C.

FILE10 IS USED TO SAVE THE SECTION X, Y, Z CORRESPONDING
LOCATION FOR A411 IN WHICH CALCULATES THE DISPLACEMENT
THICKNESS WHERE X, Y, Z SHOULD BE THE WING SURFACE LOCATION
FOR THE CURRENT RUN

FILE11 IS USED TO READ IN THE DISPLACEMENT
THICKNESS FROM A411IN

FILE12 IS USED TO REPLACE PART OF THE INPUT CARDS
BY CARD IMAGES

TAPE13 IS USED TO SAVE PART OF THE OUTPUT
SKIPPED FROM THE LINE PRINTER

TAPE14 IS USED TO SAVE THE VELOCITY POTENTIAL
FOR FUTURE USE

```
*****  
COMMON G(161,18,3),SO(161,35),VORT(115),ZV(115),  
        IV(161,35),ITE1(35),ITE2(35),  
        AO(161,18),BO(18),XO(35),YC(35),ZO(35),SCAL(35),  
        NX,NY,NZ,KTE1,KTE2,TISY,KSYK,FUS,  
        YAH,CYAW,SYAW,ALPHA,CA,SA,FMACH,N1,N2,N3,I0  
COMMON /CPF/NL  
COMMON /PCKR/ PTCK  
COMMON /FL0/P1,P2,P3/FRES,IRESJRES,KRES,ARES,EG,IG,JG,KG,AG,NSUP  
COMMON /PARMT3/ XT3(161),YT3(161),UT3(161),VT3(161),HT3(161),N01,Z  
1 COMMON /PRS/ XOD(161)  
DIMENSION XS(161,11),YS(161,11),ZS(11,11),XLE(11),YLE(11),  
        SLOFT(11),TRAIL(11),NP(11,11),E1(11),E2(11),E3(11),  
        D1(161),D2(161),D3(161),SN(161),  
        SV(161),SM(161),CP(161),XP(161),YP(161),  
        YPO(35),ZPO(35),XMAX(35),XMIN(35),YMAX(35),YMIN(35),  
        CHORD(35),SCL(35),SCD(35),SCM(35),TITLE(20),  
        FIT(3),COV(3),P10(3),P20(3),P30(3),FSMCU(3),  
1 DIMENSION RES(20),CCNT(201),PTMAP(3)
```



```

DO 12 NM=1, NME SH
C** INITIALIZE INPUT PARAMETERS WHICH HAVE RECOMMENDED PROGRAM VALUES ***
C**
C** P2C(NM) = 0.7
C** P3C(NM) = 1.0
C** FSWGO(NM) = 0.0
C** PTMAP(NM) = 0.0
C**
C** 12 READ(5,510) FIT(NM), CCOV(NM), PIO(NM)
C** READ(5,501) FMACH, YA, AL, CDO
C** READ(5,510) (ND, NS, NP, XS, YS, ZS, XLE, SLOP, TRAIL, XP, YP,
C** CALL GECH(FUS, XTEQ, CHORD, ZTIP, SWEEP, CIHED,
C** 1
C** 2 ALPHAD = AL/RAD
C** IF(BLCF .LE. 0.) GO TO 44
C** IF(PTCK .GE. 1.) WRITE(6,600)
C** READ(11) (TITLE(I), I=1,8), FMACH, ALPHAD, NS
C** DO 40 K=1, NS
C** READ(11) NFCK
C** NP(K) = NPCK1
C** NPCK1 = NPCK + 1
C** READ(11) (DUMX(NPCK1-I), DUMZ, DUMY(NPCK1-I), DELR(NPCK1-I),
C** 1
C** 1 IF(PTCK .LE. 0.) GC TC 30
C** WRITE(6,52) K, NPCK, NPCK1
C** WRITE(6,54) (DUMX(NPCK1-I), DUMZ, DUMY(NPCK1-I),
C** 1
C** WRITE(6,54) (DELR(NPCK1-I), I=1, NPCK)
C** 3C CONTINUE (XS(1,K), YS(1,K), V(1,K), I=1, NPCK)
C** CALL BLIN (XS(1,K), YS(1,K), DELR, WEIG, NPCK, NL)
C** 4C CONTINUE
C** 44 CONTINUE
C** IF(PTCK .LT. 0.) GO TC 56
C** IF(PTCK .GE. 1.) WRITE(6,600)
C** WRITE(10) (TITLE(I), I=1,8), FMACH, ALPHAD, NS
C** DO 50 K=1, NS
C** NPCK = AP(K)
C** NPCK1 = NPCK + 1
C** DO 48 I=1, NPCK
C** DUMX(NFCK1-I) = XS(I,K) + XLE(K)
C** DUMY(NFCK1-I) = YS(I,K) + YLE(K)
C** 48 CONTINUE
C** WRITE(10) NPCK
C** WRITE(10) (DUMX(I), DUMY(I), I=1, NPCK)
C** IF(PTCK .LE. 0.) GC TO 49

```



```

45 WRITE(6,52) K,NPC(K),ZS(K)
5C CONTINUE
5C ENDFILE 10
52 FORMAT(1H0,5X,3I5,F11.4)
54 CONTINUE (12F11.4)
IF (KSYM .NE. 0) YA = 0.
ISYM = ISYM - 0
IF (AL .NE. 0) ISYM = 0
YA = YA/RAD
CYA = COS(YAW)
SYA = SIN(YAW)
CA = CYA*COS(ALPHA)
SA = CYA*SIN(ALPHA)
IF (FCCT .LT. 1.) GCTC91
READ(4) NX,NY,NM,K1,K2,NIT
MX = NX + 1
MY = NY + 1
NZ = NZ + 3
DO 62 K=1,MZ
READ(4) ((G(I,J,1,1,1,I=1,MX),J=1,NY)
BUFFER CLT(N3,1)(G(I,J,1,1,1,MX),J=1,NY)
WRITE(N3,(G(I,J,0,1,1,GOTO1
IF (UNI(N3).GT.0.) GOTO1
BUFFER CLT(N1,1)(G(I,J,1,1,1,MX),J=1,NY)
WRITE(N1,(G(I,J,1,1,1,MX),J=1,NY)
IF (UNI(N1).GT.0.) GOTO1
REAC(4) (VORT(K),K=K1,K2)
REWIND N3
REWIND N1
91 CALL CCERD(NX,NY,NZ,KSym,ZTIP,XLIM,ZLM,
      SY,AX,AZ,PX,PZ,AC,BG,ZO)
1 CALL SINGL(INS,NZ,KSym,KTE1,KTE2,FUS,CHCRD0,ZS,XLE,E3,IND)
1 CALL SUFF(IND,REEP,DIHED,XO,YO,ZO,YFO,ZFC,E1,E2,E3,IND)
1 CALL SUFF(YAW,XFFEO,XLIM,FSX,NP,YS,KSym,KTE1,KTE2,IND)
2 AO,XO,ZC,SO,SCAL2,V,IV,IE1,IE2,IND
3 IF (INC.EQ.0) GCITC291
IF (FCCT .GE. 1.) GO TO 101
NM = 1
NIT = 0
CALL ESTIM
IF (LG.EQ.0) GO TO 1

```



```

REWIND N1
REWIND N1
101 IF (PTCK .GE. 1.0) WRITE (6,600)
      FGCNT = 0
      COV   = C1 V(1,NM)
      P1    = P1 O(NM)
      P2    = P2 O(NM)
      P3    = P3 O(NM)
      MIT   = F1 T(NM) + NIT
      KIT   = M1 T
      LT    = 2
      KIT = 2
      JI    = NI T
      LRES  = 0
      MRES = -NIT -2)/200
      NX   = 0
      NY   = NX +1
      NZ   = NY +2
      NY   = NZ +3
      KY   = NY +1
      K1   = 1
      K2   = NZ +1
      IF (KSYM.EQ.0) GO TO 103
      K1   = 3
      K2   = NZ /2 +1
      IF (KSYM.NE.0) L2 = 3
      IF (PTCK .LE. 0.) GC TC 108
      WRITE ('IC4')
      FORMAT ('4H0IND ICATION OF LOCATI
      1        1
      2        1
      DO 106 WRITE ('C,650) (IV(I,K),K=K1,K2)
      106 CONTINUE ('C,650) (IV(I,K),K=K1,K2)
      106 CONMAP = FTMAP(NM)
      IF (IMAF .NE. 0) GC TC 830
      WRITE ('C,600)
      WRITE ('C,112)
      FORMAT ('4SHOCHORDWISE CELL DISTR
      1        1
      DO 820 820 (C,812)
      WRITE ('C,812)
      FORMAT ('15H0 1
      1        1
      1        1
      1        1
      CALL PFXY (2,NX,A0,SO(1,ISEC))
      IF (PTCK .LE. 0.) GC TC 130
      WRITE ('C,116)

```



```

116 FORMAT(15H0 TE LOCATION ,15H PCWER LAW )
117 WRITE(6,610) XLIM,AX
118 WRITE(6,600)
119 WRITE(6,118)
120 FORMAT(4CHONORMAL CELL DISTRIBUTION IN SQUARE ROOT PLANE/
121      15H0 Y
122 DO 120 K=1,KY
123 WRITE(6,610) BC(J)
124 FORMAT(15H0 SCALE FACTOR,15H PCWER LAW )
125 WRITE(6,600)
126 WRITE(6,124)
127 WRITE(6,610) SY,AY
128 FORMAT(45H0 SPANWISE CELL DISTRIBUTION AND SINGULAR LINE/
129      15H0 X SING ,15H Y SING )
130 DO 126 K=K1,K2
131 WRITE(6,610) Z0(K),X0(K),Y0(K)
132 FORMAT(15H0 TIP LOCATION,15H PCWER LAW )
133 CONTINUE
134 WRITE(6,600)
135 WRITE(6,132)
136 FORMAT(15H0 ITERATIVE SOLUTION)
137 WRITE(6,610) MACH NO
138 WRITE(6,136) FMACH,YA,AL ,15H YAW
139 WRITE(6,610) NX,NY,NZ ,15H NY
140 WRITE(6,138) NX,NY,NZ ,15H NZ
141 FORMAT(15H0 RELAX FCT 15H RELAX FCT 2 ,15H RELAX FCT 3 )
142 WRITE(6,610) P10(NM),P20(NM),P30(NM)
143 WRITE(6,140)
144 FORMAT(10H0 ITERATION,
145      15H MAX CORRECN *4H 1 *4H J *4H K :15H AVG CORRECN ;
146      15H MAX RESIDAL *4H 1 *4H J *4H K :15H AVG RESIDAL ;
147      12H CIRCULATION,15H SONIC P(S)
148      12H CIRCULATION,15H SONIC P(S)
149 NIT = NIT +1
150 JIT = JIT +1
151 CALL MIXFLC
152 IF (IO.FC.0) GO TO 151
153 JD = 0
154 REWIND N1
155 REWIND N2
156 N1 = N2
157 N2 = N3

```



```

N3 = N
WRITE (6,66C) NIT, DG, IG, JG, KG, AG, FRES, IFES, JRES, KRES, ARES,
1 LRES = LRES +1
IF (LRES.EQ.0.MRES) LRES = 1
IF (LRES.NE.1) GO TO 143
NRES = NRES +1
COUNT (NRES) = NRES -1
RES(1:NRES) = FRES
143 IF (NM.LE.1) OR. NM.LT.MMESH) GO TO 251
IF (ABS(EG).LE. CUV) GO TO 251
148 CONTINUE
IF (NI.LT.MIT.AND.ABS(DG).GT.COV.AND.ABS(DG).LT.10.) GO TO 141
GO TO 161
151 IF (JO.EC.1) GO TO 1
REIND N1
REIND N2 = 1
JO = N3
N1 = N2
N2 = N1
GO TO 141
161 RATE = 0
IF (NRES.GT.1) RATE = (#(1. / (COUNT(NRES) - COUNT(1))) )
1 WRITE (6,162)
1 FORMAT (15H MAX RESIDUAL, 15H MAX RESIDUAL, 15H
1 15H REDUCTN/CYCLE, 15H CONV TOLERANCE)
1 WRITE (6,670) RES(1), RES(NRES), COUNT(NRES), RATE
1 * C C
1 WRITE (6,600)
DO 164 F=1,3
  BUFFER IN (N1,1) ( G(1,1,M) G(M,1,M), J=1,MY )
  READ (N1,ERR=151) ( G(1,J,M) G(M,1,M), J=1,MY )
  IF (UNI(N1).GT.0.) GO TO 151
1 CONTINUE
  LX = NX/2 +1
K = 2
KK = 0
C IF (NM.LT.MMESH) WRITE HEADER ON TAPE 8
REWIND E
REWIND S
NRC = KTE2 (TITLE(I), I=1,8), FMACH, ALPHA, NRC
C WRITE (E) (TITLE(I), I=1,8), FMACH, ALPHA, NRC
17C CONTINUE

```



```

171 KF (K*E*WZ) GO TO 191
00 172 J=1,MY
00 172 J=1,MX
G(1,J,1) = G(1,J,2)
G(1,J,2) = G(1,J,3)
C 172 BUFFER IN (NL151)(G(1,J,3),G(MX,MY,3)),J=1,MY
READ (NL151) GT,O,1 GO TO 151
C IF (UNL151) GT,O,K GT,KTE2 GO TO 171
IF (K*LL151) OR,K GT,KTE2 GO TO 171
CALL VEL0 (K,SM,CP,XP,YP,XMAX(K),YMIN(K),YMAX(K))
111 I12 IITE(K)
I12 CHCRD(K) = XP(I11)-XP(LX)
CALL FCRCF (I12) XPYP(CPAL,CHOR(E(K)),XO(K),YPO(K)),
1 KKK = KKK +1
IF (KPLCT.GT.1. AND. K.GT.KTE1) GC TC 185
IF (KPLCT.EQ.0 .AND. KKK .GT. 1) GO TO 185
WRITE (6,600)
WRITE (6,182)
FORMAT (24HOSECTION CHARACTERISTICS/
15H0 MACH NO ,15H YAW
1 WRITE (6,610) FMACH,YA,AL
1 WRITE (6,184)
FORMAT (15HOSPAN STATION 15H CL
15H CM
1 WRITE (6,610) ZPO(K),SCL(K),SCM(K)
1 Z=ZPC(K)
1 IF (WIT.LE.0) GC TC 850
1 IF (KPLCT.LE.2) CALL CPLOT (2,NX,FNACH,XP,YF,CP,SM,11,12,KPLOT)
850 CONTINUE
C WRITE CNE FILE ON TAPE 8
IF (NM.LT.1) WMESSH) GO TO 186
1 WRITE (6,NC1) XIT3(1),ZT3(1),YT3(1),UT3(1),WT3(J),I=1,NO1
NR=I2-I1+1
NR=I2-I1+1
1 WRITE CP VS X/C SECTION DATA FOR FINAL MESH ON TAPE 9
C WRITE (6,900) ZPO(K)
1 WRITE (6,910) NRD
1 WRITE (6,920) XQCD(J) CP(J) J=1,12
1 WRITEM (6,950) XQCD(J) CP(J) J=1,12
900 FORMAT (1X,20HNC,CF DATA POINTS = 15)
910 FORMAT (1X,6H X/C,8X,2HCP,7X,3HX/C,8X,2HCF,7X,3HX/C,8X,2HCF,
920 17X,3HX/C,8X,2HCF,3X)
950 FORMAT (8F10.6)
186 CONTINUE

```


C WHEN KPLOT = 2 CALL SUBROUTINE VERTEC WHICH PLOTS CP VS X/C
 C FOR EACH SECTION OF THE FINAL MESH

```

1 IF ((KPLOT.EQ.2 .AND .NM.EQ.MMESH)) CALL VERTEC(X1,X2,XOCD,CP,ARD)
   GO TO 171
191 CONTINUE
   IF (NM.EQ.1 .AND .EQ.MMESH) GO 171
   ENDFILE 8
   REWIND 6
   ENDFILE 5
   REWIND 5
20C CONTINUE
   CALL TCTFOR (KTE1,KTE2,CHORD,SCL,SCD,SCM,XC,YPO,ZPO,
   1 CD1      CL:CD1:CMR,CMY)
   CD      = CYA*CD1
   CD      = CDO+CD1
   VLC1{ABS(CD1)*GT.1.E-6) VLD1 = CL/CC1
   VLC1{ABS(CD1)*GT.0 VLD = CL/CD
   WRITE(6,60C)
   WRITE(6,192)
192 FORMAT(21H OWING CHARACTERISTICS/
   1 15H MACH NO 15H YAW
   1 15H FMACH,YA,AL
   WRITE(6,610)
   WRITET(15H) CL
   WRITET(15H) CD,CC1,CC0,CD,VLD1,VLC
   WRITET(15H) CM,YAW,15H CM_RCLL
   WRITET(15H) CMY,CMR,CMP
   1 15H CD_FORM
   1 15H L/E FORM
   1 15H CM_PITCH
   ,15H ANG OF ATTACK)
   REWIND 6
   IF ((KPLOT.LT.1) GO TO 201
   CALL RPLT(IPLCT,NRES,COUNT,TITLE,FMACH,YA,AL,NX,NY,NZ)
   CALL DRAWN(IPLCT,XMAX,YMAX,XMIN,YMIN,ZPO,FUS,TITLE,NZ,KTE1,KTE2)
   CALL TFREED(IPLCT,SV,SM,CP,XP,ZPO,TITLE,YA,AL,
   1 151
   1 IF ((ISICP.EQ.0) GO TO 151
   IF ((NX.LT.MMESH) GO TO 201
   GO TO 1
201 NX = NX +NX
   NY = NY +NY
   NZ = NZ +NZ
203 CONTINUE

```



```

CALL CCCRD (NX,NY,NZ,KSYM,ZTIP,XLIM,ZO)
1 CALL SINGL (NS,AX,AZ,PX,KTE1,KTE2,FUS,CHCRD0,ZS,XLE,YLE,
   SWEEP,DIHED,XO,YO,ZC,YFC,ZPO,E1,E2,E3,IND)
1 CALL SUFF (ND,NE,NS,NX,NZ,ISY,M,KSYM,KTE1,KTE2,SLOPf,TRAIL,
   YAW,XTEO,XLIM,FX,NP,XIV,ITE1,ITE2,
   AO,XO,ZO,SO,SCAL2,VIV,IND)
12   XP,YP,SN,C1,D2,D3,IND)
3 IF (INC.EQ.0) GC FC 291
CALL REFIN (IND,EQ,0) GO TO 221
IF (IO.EQ.0) GO TO 221
REWIND N1
REWIND N2 = FS MUC(NM)
IF (NS.MOC.LT.1) GO TO 211
DO 202 N=1,NSMCC
CALL SMCC (N1) GO TO 221
IF (IO.EQ.0) GO TO 221
REWIND N2 = N1
202 N1 = N2
N2 = N3 = NM +1
NM = 0
NIT NX = NX/2
221 NX = NY/2
NZ = NZ/2
CALL CCCRD (NX,AY,AZ,DX,KTE1,KTE2,FUS,CHCRD0,ZS,XLE,YLE,
   SWEEP,DIHED,XO,YO,ZC,YFC,ZPO,E1,E2,E3,IND)
1 CALL SINGL (NS,AY,AZ,KSYK,KTE1,KTE2,FUS,CHCRD0,ZS,XLE,YLE,
   ND,NE,NS,NX,NZ,ISY,M,KSYM,KTE1,KTE2,SLOPf,TRAIL,
   YAW,XTEO,XLIM,FX,NP,XIV,ITE1,ITE2,
   AO,XO,ZO,SO,SCAL2,VIV,IND)
12   XP,YP,SN,C1,D2,D3,IND)
3 IF (INC.EQ.0) GC FC 291
GO TO 151
251 K1 = KTE1 -1
K2 = KTE2 +1
WRITE (14) NX,NY,NZ,NM,K1,K2,NIT
DO 262 K=1,NZ
EU FFER IN {N1 1} (G(1 1 1) (G(1 1 1) G(MX,MY,1))
RE AD (N1 ERR=2 81) (G(1 1 1) (G(1 1 1) G(I,J,1))
IF JUN (N1) GT 0,1 GO TO 281
C 262 WRITE (14) (G(i,j,1),I=1,MX),J=1,MY)

```



```

REWIND 14 1 (WRT(K),K=K1,K2)
WRITE(14) 14
ENDFILE 14
REWIND 14
CALL S$ITCH(1,I$TOP)
CALL SLICE(1,I$TOP)
IF(I$TOP.EC.1) GO TO 161
J17 (N11.LT.=0.MIT.AND.ABS(DG).GT.COV.AND.ABS(DG).LT.10.) GC TO 141
GO TO 161
281 REWIND 4
GO TO 151
291 WRITE(6,6001)
WRITE(6,2921)
292 FORMAT(24H0BAD DATA,SPLINE FAILURE)
GO TO 1
301 CONTINUE
REWIND 10
REWIND 11
IF(KPLC1.GT.0) CALL PLOT(0.,0.,999)
C
50C FORMAT(1X)
51C FORMAT(8F10.6)
53C FORMAT(2CA4)
55C FORMAT(1H1)
60C FORMAT(F12.5,7G15.5)
61C FORMAT(1H0,720A4)
63C FORMAT(18.7115)
64C FORMAT(1X,3313)
65C FORMAT(10E15.5,2E15.5,3I4,E15.5,F10.5,I10,F10.3)
66C FORMAT(2E15.4,2F15.4,E15.4)
67C FORMAT(2E15.4,2F15.4,E15.4)
END

```



```

C **SUBROUTINE BLIN*****
SUBROUTINE BLIN (XT,YT,DELR,WEIG,N,AL)
C
C SUBPROGRAM FOR NORMALLY ADDING THE DISPLACEMENT
C THICKNESS TO THE ORIGINAL WING SECTIONS
C
XT:   CONTAIN THE X COORDINATES OF THE ORIGINAL
      WING SECTION WHEN CALLED
      CONTAIN THE X COORDINATES OF THE DISPLACED
      WING SECTION ON RETURN
YT:   CONTAIN THE Y COORDINATES OF THE ORIGINAL
      WING SECTION WHEN CALLED
      CONTAIN THE Y COORDINATES OF THE DISPLACED
      WING SECTION ON RETURN
C
DELR:  THE DISPLACEMENT THICKNESS
C
COMMON /FCR/ PTCR
DIMENSION XT(1),YT(1),DELR(1)
WRITEN(6,1000)
I = 1
XT = XT(1)
YT = YT(1)
DELR = 0.0
1000 IF (I .EQ. N) GO TO 300
      IF (I .EQ. I+1) GO TO 400
      IF (I .EQ. I-1) GO TO 500
      XT = XT + DELR
      YT = YT + DELR
      I = I + 1
      GO TO 1000
300  XT = XT + DELR
      YT = YT + DELR
      I = I + 1
      GO TO 1000
400  XT = XT - DELR
      YT = YT - DELR
      I = I - 1
      GO TO 1000
500  XT = XT - DELR
      YT = YT - DELR
      I = I - 1
      GO TO 1000
      IF (ABS(XT) .LT. 1.0E-6) GO TO 600
      DYX = -(YT-X23)/(X12*X31)*Y1
      DYY = (X12-X23)/(X31*X23)*Y2
      DDX = (X12-X31)/(X31*X23)*Y3
      IF (ABS(DYX) .LE. 1.0E-6) GO TO 700
      DYX = -1.0/DYX
      GO TO 700
      DDX = -1.0/DDX
      GO TO 700
      DYY = -1.0/DYY
      GO TO 700
      CONTINUE
      IF (I .EQ. N) GO TO 800
      CONTINUE
SI = 1.

```



```

IF (I•LT•NL) SI = -1.
GO CONTINUE
S = O•
DL = DELL(I)
DX = O•*SI
GO TO EEC
CONTINUE
S = SQRT(S)
S = 1./S
F = (DY*XN*S*SI.LT.C.) F = -1.
IF (DY*XN*S*SI.LT.C.) F = -1.
DL = S*F
DX = ABS(DYXN)*S*SI
DX = DX*DL
DY = DY*DL
XT(I) = X2 + DX*WEIG
YT(I) = Y2 + DY*WEIG
CONTINUE
IF (PTCK,IC00),1,1 GO TO 890
IF (ITE(C,IC00),1,F,S,DL,DY,DYXN,XT(I),YT(I),CYX,WEIG
IF (I•EC..N) GO TO 900
X1 = X2
Y1 = Y2
X2 = X3
Y2 = Y3
I = I+1
GO TO 2CO
CONTINUE
RETURN
FORMAT (1H ,15,F7.2,9G13.5)
END

```



```

C**SUBROUTINE PPXY*****PPXY (I1,I2,X,Y)
C SUBROUTINE FCR LINE PRINTER PLOTTING CF THE UNWRAPPED
C WING SECTIONS
C
COMMON /PCKR/ TICK
COMMON /SHARE/ LINE(100)
DIMENS(X(1),Y(1))
DATA IB /1H/, IP /1H+/, KMAX /100/, ACC /1.5/,
     IZ /1H/, CONST /0/
1 DO 10 I=1,100
LINE(I) = IB
CONTINUE
1C YMAX = -1.0E35
YMIN = -YMAX
WICTH = KMAX - 5
DO 20 I = 1,12
YMAX = AMAX(YMAX,Y(I))
YMIN = AMIN(YMIN,Y(I))
2C CONTINUE
VAL = ABS(YMAX) + ABS(YMIN)
S = WICTH/VAL
KK = 0
IF (CONST.LE.0) LINE(KK)=IZ
IF (KK.NE.0) LINE(KK)=IZ
DO 30 I=1,12
K = S * (YMAX-Y(I)) + ADD
IF (K.LT.1) K = 1
IF (K.GT.KMAX) K = KMAX
LINE(K) = IP
WRITE(6,100) I,X(I),Y(I),LINE
LINE(K) = IB
IF (K.EQ.K) LINE(K) = IZ
30 CONTINUE
RETURN
10C FORMAT (1X,13,2F10.4,4X,100A1)
ENC

```



```

C**SUBROUTINE LSQR(NL,NB,XP,YP,XSING,YSING)
C
C SUBPROGRAM FOR WING SECTION LEADING EDGE SINGULAR POINT
C CALCULATION BY MEANS OF COMPUTING THE FOCUS OF A
C PARABOLA BY NB * 2+1 POINTS LEAST-SQUARE FIT CENTERED AT
C THE LEADING EDGE
C
NB : SUPPLY BY THE CALLING PROGRAM GEOM

COMMON /FCKR/ FTCK
DIMENSION XP(1),YP(1)
N1 = NL - NB
N2 = NL + NB
N3 = N2 - N1 + 1
A1 = N1
B1 = 0
C1 = 0
A2 = 0
B2 = 0
C2 = 0
A3 = 0
B3 = 0
C3 = 0
D1 = 0
D2 = 0
D3 = 0
SCALE = 100.
SCALE2 = 50.
DO 300 I = NI * N2
YY = (YP(I) - YP(NL)) * SCALE
BI = B1 + YY
YP2 = YP(I) + YY
C1 = C1 + YP2
YP3 = YP2 * YY
C2 = C2 + YP3
YP4 = YP2 * YY
C3 = C3 + YP4
XX = XP(I) * SCALE2
D1 = D1 + XX
YY = YY + XX
D2 = D2 + YY
Y2X = YP2 + XX
300 D3 = D1
A2 = C1
B2 = C1
A3 = C2
B3 = C2

```



```

FA1 = B2*C3 - B3*C2
FA2 = A2*B3 - A3*B2
FA3 = A1*FA1 + B1*FA2 + C1 *FA3
DET = 1 / CDET
DI = 1 *FA1*C1
FA1 = FA2*D1 - B1*(C3)*D1
FA2 = (A1*C3 - A2*B3)*D1
FA3 = ((A1*C2 - A2*C1)*D1
FB1 = ((A1*B2 - A2*B1)*D1
FB2 = (A1*C1 + FB2*D2 + FC1*D3
FB3 = FA1*D1 + FB3*D2 + FC3*D3
FC1 = FA2*D1 + FB3*D2 + FC2*D3
FC2 = FA2*C1 + FA2*D2 + FC3*D3
FC3 = FA2*C2 + FA2*D2 + FC4*D3
FA = FA2*C2 + FA2*D2 + FC4*D3
FB = FA2*C2 + FA2*D2 + FC4*D3
FC = FA2*C2 + FA2*D2 + FC4*D3
FA = A / SCALE2
FB = C / SCALE2
FC = C * SCALE**2
XSING = A + (1 / C - E**2) * 25/C
YSING = -B * (5 / C + YP(NL))
IF (PT CK = 400) N GO TO 520
WR1TE ('1H05X' LEAST SQUARE FIT, /)
FORMAT FCIINT$LEAST-SQUARE FIT, /)
1 WR1TE ('E1500') A1,B1,C1,D1
WR1TE ('E1500') A2,B2,C2,D2
WR1TE ('E1500') A3,B3,C3,D3
WR1TE ('E1500') FA1,FB1,FC1
WR1TE ('E1500') FA2,FB2,FC2
WR1TE ('E1500') FA3,FE3,FC3
WR1TE ('E1500') FSING,YSING,A,B,C,DET,DI
FORMAT ('10G13.5')
CONTINUE
R2=0.
DXAM = C.
DXZN = C.
DO 650 1 = NL N2(KL)
Y = YP(1) - YP(KL)
X = A + B*Y + C*Y**2
DX = X - XP(1)
DX2 = CX*DX
R2 = R2 + DX2
DXA = ABS(DXA)
IF (DXAN.GE.DXA) GC TO 600

```



```

DXAM = CXA
DXAM = EXAM**2
DX2M = EXAM**2
CONTINUE
IF (PTCK .LE. 0.) GC TC 65C
WRITE(6,700) 1,X,Y,DX,DX2,R2,DXAM,DX2Y,XP(1),YP(1)
70C CONTINUE
IF (PTCK .LE. 0.) GC TC 75C
RA = R2/A1
WRITE(6,700) N'RA',DXA
75C FORMAT(113,9G13.5)
CONTINUE
RETURN
ENTRY LSC
IF (DXA .LE. 1. E-4) RETURN
WRITE(6,800) DXAM
80C FORMAT(1F0.5X,'WARNING ?? DEVIATION OF THE LEADING EDGE POINTS',
1   ' FROM PARABOLA IS GREATER THAN 0.C001',/6X,'DXAM = ',G13.4/)
END

```



```

C** SUBROUTINE GEOM***** (ND,NS,NP,XS,YS,ZS,XLE,YLE,SLOP,TAIL,XF,YF,
SUBROUTINE GEOM (ND,NS,NP,XS,YS,ZS,XLE,YLE,SLOP,TAIL,XF,YF,
1 FUS,XTE,OCH,DO,ZTIF,SWEEP,DIHED,
2 FIX,PX,PZ,ISYMO,KSYM)

```

C GEOMETRIC DEFINITION OF WING

STANDARD BOEING INPUT FORMAT FOR WING SECTION DATA IS USED
OPTION FOR WING SECTION TRAILING EDGE CLOSURE ANGLE
AND BISECTOR SLCP BE AUTOMATIC COMPUTED IS AVAILABLE
LEADING EDGE SINGULAR POINT CAN BE AUTOMATIC COMPUTED
BY INVOKING THE OPTION TO CALL LSQR

```

COMMON /PCKR/ PTCK
COMMON /CF/ NL
COMMON /CFF/ NL
DIMENSION XS(ND),YS(ND),ZS(ND),XLE(1),YLE(1),NP(1),
1 SLOP(1),TAIL(1),XP(ND),YP(ND),NP(1),
*** **** *** **** *** **** *** **** *** **** *** **** *** ****
C** INITIALIZE INPUT PARAMETERS WHICH HAVE RECOMMENDED PROGRAM VALUES ***
C** FNE = 2.0
C** PX = 0.0
C** PZ = 0.0
C** FX = 0.0
C** TRL = 0.0
C** SLT = 0.0
C** XSLING = 0.0
C** YSLING = 0.0
C** YSYM = 0.0
C** RAD = 57.29579513082
C** READ (E,50) (E,510) ZSYM,FNS,FNS,DIHED,FUS
C** IF (FNS.LT.3.) RETURN
C** KSYM = ZSYM
C** IF (FUS.GE.0.) KSYM = 1
C** NS = FNS
C** WRITE (6,2) FNS
2 FORMAT (15HO) FUSELAGE RAD )
C** WRITE (6,10) FLS
C** WRITE (6,4) FLS
C** FORMAT (15HO) SWEEP DIHED ,15H   CIHEC   )
4 WRITE (6,610) SWEEP DIHED ,15H   CIHEC   )
C** SWEEP = SWEEP/RAD
DIHED = DIHED/RAD

```



```

ISYNO = 1.
XTEC = 0.
CHORDO = 0.

11 READ (5,50) ZSIK, XL, YL, CHORD, THICK, AL, FSEC
READ (5,51) ZS1 = ZS(1)
IF (K .EQ. 1) ZS1 = 2S(1)
ALPHA = AL/RAD
IF (K .GT. 1) AND .EQ. 0.) GO TO 31
READ (5,50) FN
READ (5,51) FN
N = FN
READ (5,500)
NL = N + 1
READ (5,501) (XP(N-1), YP(N-1), I=1,N)
FORMAT (6F10.0)
DO 26 I=1,N
IF (XP(I+1)-XP(I)) .LT. 0.01 GO TO 26
NL = I
GO TO 800
CONTINUE
CON IF (NE .LE. 0.) GC TO 21
DXL = YF(1) - YF(2)
DXL = XF(1) - XP(2)
DYU = YF(N) - YP(N-1)
DXU = XF(N) - XP(N-1)
TSU = CYL/DXU
TSL = CYL/DXL
TRL = ATAN2(DYL,DXL) - ATAN2(DYU,DXU)
TRL = TRL*RAD
SLT = TSL+TSU)*.5
NB = FNE
CALL LSCA (NL, NE, X, P, YP, XSING, YSING)
21 WRITE (6,600)
WRITE (6,622) ZSIK
FORMAT (16H0) PROFILE AT Z = 15H .5/ TE SLCE
15H0 TE ANGLE Y SING
15H Y SING
22 FORMAT (16H0) TRL, SLT, X SING, Y SING
15H0 AT Z = 15H .5/ TE SLCE
15H Y SING
23 WRITE (6,610) TRL, SLT, X SING, Y SING
24 FORMAT (6,620) NL, X, P(NL), YP(NL), XP(NL)
25 FORMAT (2X,5 (2F10.5,4X)) 1
26 SCALE = CHORD (XP(1) - XP(NL))
27 XLE(K) = XL + (XSING - XP(NL))*THICK*SCAL
62C FORMAT (2F10.5,4X)) 1
28 YLE(K) = YL + (YSING - YP(NL))*THICK*SCAL
29 XX = XP(NL) + (XSING - XP(NL))*THICK
30 YY = YP(NL) + (YSING - YP(NL))*THICK

```



```

CA = COS(ALPHA)
SA = SIN(ALPHA)
DO 32 I=1,N
XS(I,K) = SCALE*((XP(I)-XX)*CA+THICK*(YP(I)-YY)*SA)
YS(I,K) = SCALE*((THICK*(YP(I)-YY)*CA-(XP(I)-XX)*SA)
32 SLOP(I,K) = THICK*SLT-TAN(ALPHA)
TRAIL(K) = THICK*TRL/RAD
NP(K) = N
CHORDO = AMAX1(CHORD,ALPHA*NE*0.) ISYMC = C
IF (YS YP LE 0.0*CR*ALPHA*NE*0.) ISYMC = C
32 WRITE(6,42) Z(K)
42 FORMAT(2F10.5)
15H SECTION XLE 15H
15H TICKNESS RATIO 15H
15H WRITE(6,610) XLYL,CHRD,THICK,AL
YMIN = YP(NL)
YMAX = YMIN
DO 44 I=1,N
IF (YP(I) .GE. YMIN) GO TO 43
YMIN = YF(I)
JMAX = YP(I)
43 IF (YP(I) .LE. YMAX) GO TO 44
JMAX = YP(I)
YMAX = YP(I)
NN = N - 1
SUM = C
DO 46 I=NL,NN
SUM = SUM + .5*(YP(I)+YP(I+1))*(XP(I+1)-XP(I))
46 CONTINUE
NM = NL - 1
DO 48 I=1,NM
SUM = SUM + .5*(YP(I)+YP(I+1))*(XP(I+1)-XP(I))
48 CONTINUE
30C FORMAT(15H MAX YMIN ,15H YCLF ,15H AREA ,YMAX)
1 WRITE(6,320) YMIN;JMIN;YMAX;JDIF;SUM
320 FORMAT(1H ,612*4,111,G19.4,I11,G19.4,G15.4)
CALL SC
IF (FUSS LE 0.) GO TO 61
R = AMAX1(0.0*(FLS*2-ZLE(1)*2))
Z = ZS(K)-2S1+SQRT(R)
R = FUS*2/(YLE(K)**2+Z**2)
ZS(K) = Z*(1.-R)
YLE(K) = YLE(K)*(1.+R)
S = R*XSC(NL,K)

```



```

XLE(K) = XLE(K) - S
DO 52 I=1,N
XS{I,K} = XS{I,K}*{1. + S
52 YS{I,K} = YS{I,K}*{1. + R}
61 K IF (K.LE.NS) GO TO 11
1F (KS)YR*NE*01 5*(ZS(1) + ZS(NS))
Z0 (KS)YR*NE*01 20 = ZS(1)
DO 62 K=1,NS
XTFO = AMAX1(XTE0,XS(1,K))
ZS(K) = ZS(K) - Z0
62 ZT1P = ZS(NS)
RETURN
500 FORMAT(1X)
510 FORMAT(1H1)
600C FORMAT(F12.4,7F15.4)
610C FORMAT(F12.4,7F15.4)
ENC

```



```

C***SUBROUTINE COORD(NX,NY,NZ,KSYM,ZLIM,XLIM,ZLIM,
1      SY,AZ,PX,PZ,AO,B0,Z0)
C      SETS UP STRETCHED PARABOLIC AND SPANNING COORDINATES
C      DIMENSION = AO(1) B0(1) Z0(1)
PI = 3.1415926535898
BOUND = .95
AX = .5
AY = .5
AZ = .5
XLIM = .625*BUND
ZLIM = .625*BUND
SY = .5
SCALZ = 2*T1F/(1.000001*ZLIM)
LX = NX/2+i
DX = NX/2+1
Q = PI/XLIM
QR = PX/C
R = 1.0/(1.0 + R*SIN(Q)) -XLIM
DO 12 I=1,NX
C = ((I -LX)*DX
DIF = ABS(D)*LE.XLIM/GD.T0 12
B = 1.0
IF (D.LT.0.) B = -1.0
A = A**AX
C = B*XLIM + (D - B*XLIM)/C
12 A0(I) = NY+1
DY = BOUND/NY
DO 22 J=1,KY
D = ((KY -J)*DY
A = 1.0 -D*D
C = A**AY
SY*D/C
22 BO(J) = NZ/2+1
K1 = NZ/2+1
K2 = NZ/2+1
DZ = PZ/C
Q = (KSYM.EQ.0) GO TC 31
LZ = NZ+3
K1 = NZ+3
K2 = NZ+3
DZ = BOUND/NZ

```



```

31      Q = Q + Q
      R = -PZ/Q
      K = K1 + K2
      D = (K - LZ)*DZ
      D = D + R*SIN(G*D)
      IF (ABS(C) > ZLIM) GOTO 32
      B = 1.0
      IF (D < 0.0) B = -1.0
      A = A**AZ
      C = B**ZLIM - (C - B*ZLIM)*E)**2
      D = SCALZ*C + (D - B*ZLIM)/C
      ZO(K)
      RETURN
END
32

```



```

C** SUBROUTINE SINGL* *****
SUBROUTINE SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHORDO,ZS,XLE,YLE,
1 GENERATES SINGULAR LINE FOR SQUARE ROOT TRANSFORMA-
DI MENSION ZS(1),XLE(1),YLE(1),XO(1),YO(1),ZP0,E1,E2,E3,IND)
1 K1 = 1
K2 = NZ +1
IF (KSYM.EC.0) GO TO 11
K1 = 2
K2 = NZ +3
KTE1 = 3
11 DO 12 K=K1,K2
IF ((ZO(K).LT.ZS(1)),KTE1 = K
IF ((ZC(K).LE.ZS(NS)),KTE2 = K
12 CONTINUE
CALL SPLIF (1,NS'Z'S'XLE,E1,E3,Z'0'0'0'E1,E2,E3,IND)
CALL INTPL (KFE1'K'TE2'Z'0'X'1,NS,Z'0'X'1,NS,Z'0'X'1,SWEEP)
SS1 = CHORDO*EL(1)
= CHORDO*EL(NS)
= CHORDO*EL(NS)
CALL SPLIF (1,NS'Z'S'YLE,E1,E2,E3,Z'0'Y'1,NS,Z'0'Y'1,NS,Z'0'Y'1,IND)
CALL INTPL (KFE1'K'TE2'Z'0'Y'1,NS,Z'0'Y'1,NS,Z'0'Y'1,NS,Z'0'Y'1,IND)
T1 = CHORDO*EL(1)
= CHORDO*EL(NS)
T2 = X0(KTE1) + X0(KTE1) - X0(KTE1+1)
YO(KTE1-1) = YC(KTE1) + YO(KTE1) - YO(KTE1+1)
IF (KSYM.NE.0) GO TO 31
N 22 K=K1,N = KTE1-1
DU 22 K=K1,N = (ZO(K) - ZO(KTE1)) / CHORDO
ZZ = EXP(ZZ)
A 22 X0(K) = X0(KTE1) + S*ZZ - (S1 - T1)*(1. - A)
YO(K) = YO(KTE1) + T*ZZ + (T2 - S1)*(1. - A)
31 N 32 K=N,K2 = (ZO(K) - ZO(KTE2)) / CHORDO
ZZ = EXP(-ZZ)
A 32 X0(K) = X0(KTE2) + S*ZZ + (S1 - T1)*(1. - A)
YO(K) = YO(KTE2) + T*ZZ + (T2 - S1)*(1. - A)
DO 42 K=K1,K2
YP0(K) = YO(K)
ZPC(K) = ZO(K)
IF (FUS.LE.C.) GC TC 42
A = .25*(Z0(K)*2 - YO(K)**2) + FUS**2
B = .5*Z0(K)*YO(K)
S = SQRT(A**2 + B**2)

```



```
IF (S.G1.C. = 0.T = 5*ATAN2(B,A)
S = SQR(T(S))
YPO(K) = .5*YO(K) + S*SIN(T)
ZPO(K) = .5*ZO(K) + S*COS(T)
CONTINUE
RETURN
END
```

42


```

C** SUBROUTINE SURF*****
SUBROUTINE SURF (ND,NE,NS,NX,NZ,ISYM,KSYM,KTE1,KTE2,
YAW,XTE0,XLIM,FXNP,XSYSLCP1,TRAIL,
AO,XO,ZO,SO,SCAL,ZV,IV,IE1,IE2,
XP,YP,SURFACE,AI,NE,SH,POINTS
S(NE,1),XS(ND,1),YS(ND,1),ZS(1),SLOP1(1),
AO(1),XO(1),ZO(1),SCAL(1),ZV(1),
XP(1),YP(1),SN(1),D1(1),D2(1),D3(1),
IV(NE,1),NP(1),ITE1(1),ITE2(1),
3*1415926535896
= TAN(YAW)
= XTE0/XLIM**2
DX = 2*X/NX +1
MX = NX +1
MZ = NZ +3
IV0 = 1 -ISYM -ISYM -ISYM
IV1 = -1 -ISYM -ISYM -ISYM
DO 2 K=1,NZ MX
ITE1(K) = MX
ITE2(K) = MX
DO 2 I=1,NX
IV(I,K) = -2
2 SO(I,K) = 0
KTE1 = KTE1
K2 = 1 +1
K2 = K2 -1
R2 = 1*20(K) ) 21 S(K1) 23/(2S(K2) -2S(K1))
2 R2 = 1*(-R2 / (I3*NX)/16 +1
R1 = NX +2 -12
IF (FIX*EQ*C) GO TO 31
IF (R1*X(C,1/K1) +R2*X(S(1,K2)
CC = SQRT(C,1/S0)
DO 26 I=2 NX
IF ((AC(1) + 5*DX)*LT*CC) 11 = 1 +1
IF ((AC(1) - 5*DX)*LT*CC) 12 = 1
26 CONTINUE
31 KK = K1
RR = NP(KK)
41 ANGL = PI +PI
U = 1*
V = 0*

```



```

DO 42 I=1,N
R = SQRT(XS(I,KK)*#2 +YS(I,KK)*#2)
IF (R .EQ. 0.) GO TO 43
ANGL = ATAN2((U*YS(I,KK) -V*XS(I,KK))
              (U*XS(I,KK) +V*YS(I,KK)))
1 U = XS(I,KK)
= YS(I,KK)
= SQRTR(R +R)
= R*CCS(.5*ANGL)
= R*SIN(.5*ANGL)
XP(I) = PI
YP(I) = 0.
GO TO 42
42 ANGL = PI
= -1.
= 0.
= 0.
42 CONTINUE = AO(12)/AMIN1(ABS(XP(1)),ABS(XP(N)))
SS = .5/S**2
DO 44 I=1,N
XP(I) = S*XF(I)
YP(I) = S*YF(I)
ANGL = ATAN(SLOPT(KK))
ANGL1 = ATAN(YS(N,KK)/XS(N,KK))
ANGL2 = ATAN(YS(N,KK)/XS(N,KK))
ANGL1 = ANGL -.5*(ANGL1 -TRAIL(KK))
ANGL2 = ANGL -.5*(ANGL2 +TRAIL(KK))
ANGL = TAN(ANGL1)
T2 = TAN(ANGL2)
CALL SPLIF((1,N,XP,YP,D1,D2,D3,T1,T2,O,IND)
IF (INC(O) WRITE(6,500) KK,K1,K2,N,FR,R1,R2,ZS(KK))
500 FORMAT(12HOBAC MAPING,4,10,4,13,4)
CALL INITL((1,12,A0,S1,1,N,XP,YP,C1,D2,D3,C)
X1 = .25*XS((1,KK)
A = SLOFT(KK)*(XS((1,KK) -X1))
B = 1/(XS((1,KK) -X1))
ANGL = PI
= PI
= 1.
= 0.
= 1.
= 0.
= 1.
= -1.
44 XF(I) = SS*AO(I)**2
YF(I) = B*((XX -X1) +A*ALOG(D)/D
R = SQRTR(XX**2 +YY**2)
ANGL = ATAN2((UU*YY -V*XX), (U*XX +V*YY))
ANGU = XX
= YY

```



```

52 SN(I)          R*SCRT(R,+R)
      A          = R*SIN(.5*ANGL)
      B          = SLCFT(KK)*(XS(N,KK)-X1)
      ANGL       = 0.
      U          = 1.
      V          = 0.   +1
      M          = 12   +1
      DO 54 I=N,NX SS*AO(1)**2
      XX          = B*(XX-X1)
      D          = YS(N,KK)+A*ALOG(D)/D
      YY          = SQR(X**2+Y**2)
      R          = ANGL+ATAN2((U*YY-V*XX),(U*XX+V*YY))
      ANGL       = XX
      U          = YY
      V          = S*SCRT(R,+R)
      R          = R*SIN(.5*ANGL)
      DO 54 I=2,NX
      E2          = SO(I,K)
      DO 62 I=K,EC.K2) SO(I,K)
      KK          = K2
      RR          = R2
      GO TO 41
      SS          = SSO
      IF (FIX.EQ.0.) = (R1*XN(1,K1) + R2*XS(1,K2)) / (AO(11)*2 - SO(11,K)*2)
      1SSCAL(K)  = SS+SS
      ITIE1(K)   = I1
      ITIE2(K)   = I2
      ZV(K)       = ZO(K) - TYAH*(X0(K) + SS*AC(11)*AO(11))
      DO 72 I=11,I2
      IV(I,K)    = I2
      M          = I1   -1
      DO 74 I=1,N
      ZZ          = ZO(K)
      IF (ZZ*EE.ZV(KTE1)) - TYAH*(X0(K) + SS*AO(11)*AO(11))
      CONTINE    = IVO
      M          = I2   +1
      DO 76 I=N,NX
      ZZ          = ZO(K)
      IF (ZZ*EE.ZV(KTE1)) - TYAH*(X0(K) + SS*AO(11)*AO(11))
      CONTINE    = K2   -1
      K2          = K
      IF (K.LE.KTE2) K2   +1
      IF (K.LE.KTE2) GC  IC 21
      K1          = 2
      K2          = NZ

```



```

IF (KSYM.EC.0) GC TC 81
K1 = 3
K2 = NZ +2
81 SCAL(K) = SCAL(KTE2)
DO 82 I=1, MX
Z2 IF (Z2.LE.ZS(NSI).AND.ZZ.GE.ZV(KTE1)) IV(I,K) = IV0
82 CONTINUE
K IF (K.LE.K2) GO TO 81
SCAL(K) = SCAL(KTE2)
N IF (YA0.LE.0) GO TO 93
10 DO 92 I=10,LX
N ZV(N) = ZO(KTE2) - TYAW*(X0(KTE2) - SS*A0(I)*A0(I))
92 ZV(KTE1-1) = ZO(KTE1) - TYAW*(XC(KTE1) + SS*A0(I)*A0(I))
ZV(N+1) = ZO(KTE2+1)
DO 102 K=K1,K2
DO 104 I=2,MX
IF (IV(I,K)*GT.0) GC TC 104
IF (IV(I+1,K+1)*GT.0.OR.IV(I-1,K+1)*GT.C) IV(I,K) = IV1
IF (IV(I+1,K-1)*GT.0.OR.IV(I-1,K-1)*GT.C) IV(I,K) = IV1
104 CONTINUE
102 IF (SO(LX,K)*LT.1.E-05) IV(LX,K) = 0
IF (KSYM.NE.0) RETURN
N DO 112 K=1,N
112 SCAL(K) = SCAL(KTE1)
RETURN
END

```


C** SUBROUTINE ESTIM*****
SUBROUTINE ESTIM

C INITI AL ESTIMATE OF REDUCED POTENTIAL
COMMON G(161,18,3),SO(161,35),VORT(115),ZV(115),
IV(161,135),ITE1(35),ITE2(35),ITE2(35),
AO(161),BO(118),XO(35),YC(35),ZC(35),SCAL(35),
NX,NY,NZ,KTE1,KTE2,ISYM,FUS,MKS,
YAW,CYAH,SYAW,ALPHA,CA,SA,FACH,N1,N2,N3,IC
MX = NX +1
MY = NY +2
MZ = NZ +3
DO 12 I=1,161
DO 12 J=1,1E
DO 12 K=1,3
12 G(I,J,K) = 0.
DO 22 K=1,MZ
WR ITE(N3) ((G(I,J,1),I=1,MX),J=1,NY)
WR ITE(N1) ((G(I,J,1),I=1,MX),J=1,NY)
22 CONTINUE
K1 = KTE1 -1
K2 = KTE2 +ITE2(KTE2) -NX/2
DO 32 K=K1,K2
32 VORT(K) = 0.
10 RETURN
END


```

C** SUBROUTINE MIXFLO *****
C      SUBROUTINE FOR MIXED SUBSONIC AND SUPER SONIC FLOW
C      SOLUTICN OF EQUATIONS FOR MIXED FLOW
C      USING FINITE VOLUME SCHEME
COMMON G(161:183),SO(161:35),VOR(115),ZV(115),
     1 IVE(35),ITE1(35),ITE2(35),
     2 IO(161:18),BO(18),XO(35),YC(35),ZO(35),SCAL(35),
     3 AX,NY,NZ,KTE1,KTE2,ISYM,KSYN,FUS,
     4 YAW,CY,Aw,SYAW,ALPHA,CA,SA,FMACH,N1,N2,N3,I0
COMMON /SPAY/ GL(161:18),QQL(161:18),FL(161:18),
     1 GL(161:18),VL(161:18),LL(161:18),
     2 AL(161:18),BL(161:18),CL(161:18),
     3 RESL(161:18),
P1,P2,P3,FRES,IRES,JRES,ARES,DG,JG,KG,AG,NSUP
COMMON /FLC/
COPMON/SyP/
LX=NX+1
PX=NX+1
KY=NY+1
MY=NY+1
JJ=2
J1=(FMACH*GE-1)*J_1=3
TY_Aw=SYAw/G_YAW
FMACH2=FMACH**2
AA0=1.0/FMACH**2+.2
C1=2./F1
Q2=1./F2-1.
TOT=0.
FRES=0.
ARES=0.
DG=0.
AG=0.
NSUP=0.
K1=3
K2=NZ+2
IF(KSYN.EQ.1) GO TO 1
K1=2
IF(FMACH*GE-1.) K1 = 3
K2=NZ
DO 2 M=2,3
READ(N1,ERR=101) ((G(I,J,M),I=1,MX),J=1,MY)
CONTINUE
K=1
NV=KTE1-1
RV=2.
DO 12 J=1,MY
DO 12 I=1,MX
G(I,J,1)=G(I,J,2)

```



```

00L(I,J) = 0.
FL(I,J) = 0.
UL(I,J) = 0.
BL(I,J) = 0.
AL(I,J) = 0.
CL(I,J) = 0.
RE SL((I,J)) = 0.
IF(KSYR=NE.O) GO TO 21
CALL YSHEEP = 1.
RV GO TO 51
DO 22 J=1,MY
G(I,J,2) = G(I,J,3)
GL(I,J,2) = G(I,J,3)
READ (N1,ERR=101) ((G(I,J,1), (G(I,J,3)), I=1,MX), J=1,MY)
WRITE (N2) ((G(I,J,1), (G(I,J,3)), I=1,MX), J=1,MY)
K GO TO 51
31 CALL YSHEEP
RV IF (K*NE*KTE2*OR(YAH+LE,0.0) +1
10 DO 42 I=10,LX
M NV = NV +1
VORT(NV) = VORT(NV) + P3*(V - VORT(NV))
51 IF (K*EC,K2) GO TO 61
DO 52 J=1,MX
G(I,J,1) = G(I,J,2)
G(I,J,2) = G(I,J,3)
READ (N1,ERR=101) ((G(I,J,1), (G(I,J,3)), I=1,MX), J=1,MY)
WRITE (N2) ((G(I,J,1), (G(I,J,3)), I=1,MX), J=1,MY)
K GO TO 51
61 DO 62 N=2,3
WRITE (N2) ((G(I,J,M), I=1,MX), J=1,MY)
62 CONTINUE
FRES = FRES/64.*TOT
ARES = ARES/64.*TOT
AG = AG/TOT
10 RETURN = 0
101 10

```


RETURN
ENC


```

B = 5*2M(I)*YM(I)
= SQR(T(A**2 +B**2)
I = 0*I = 5*ATAN2(B,A)
IF ((B*EC.O.*AND.YM(I).LT.(FS+FS)) T = 5*FI
IF ((B*EC.O.*SQR(I*S) +S*SIN(T)
S = 5*YM(I) +S*COS(T)
YM(I) = 5*ZM(I) +S*COS(T)
ZM(I) = 25*(ZRM(I)**2 -YRM(I)**2) +FS**2
A = 5*ZRM(I)*YRM(I) +FS**2
B = 0*SQRT(A**2+B**2)
T = SQRT(S) ATAN2(B,A)
S = SQR(1-S) = 5*YRM(I) +S*SIN(T)
YRM(I) = 5*ZRM(I) +S*COS(T)
ZRM(I) DO 22 I=1,N X
24 XX
1 XY = XR(I+1) +XR(I+1) -XR(I+1) -XR(I+1)
1 XZ = XR(I+1) +XR(I+1) -XR(I+1) -XR(I+1)
1 YX = XR(I+1) +XR(I+1) -XR(I+1) -XR(I+1)
1 YY = YR(I+1) -YR(I+1) +YR(I+1) +YR(I+1)
1 YZ = YR(I+1) +YR(I+1) +YR(I+1) +YR(I+1)
1 ZX = -ZR(I+1) -ZR(I+1) +ZR(I+1) +ZR(I+1)
1 ZY = +ZR(I+1) +ZR(I+1) -ZR(I+1) -ZR(I+1)
1 ZZ = -ZR(I+1) +ZR(I+1) +ZR(I+1) +ZR(I+1)
1 FX X = YY*ZZ -YY*ZX -YY*ZY -YY*XZ
1 FY X = YX*ZX -YX*ZY -YX*XY -YX*YZ
1 FZ X = ZX*ZY -ZX*XY -ZX*YY -ZX*YZ
1 FX Y = YY*ZY -YY*XY -YY*YY -YY*YY
1 FY Y = YX*ZY -YX*XY -YX*YY -YX*YY
1 FZ Y = ZX*XY -ZX*YY -ZX*YY -ZX*YY
1 FX Z = YY*XY -YY*YY -YY*YY -YY*YY
1 FY Z = YX*XY -YX*YY -YX*YY -YX*YY
1 FZ Z = ZX*YY -ZX*YY -ZX*YY -ZX*YY
FM(I) = FX*X**XX +FY*X**YY +FZX*XZ
A = 1*/FM(I) -G(I,J,2) +G(I+1,J+1,2) -G(I,J+1,J+2)
GX

```



```

UV WQL(I,J) +UL(I,J)
BV *(VR +VL(I,J))
CV *(WR +WL(I,J))
QR FR
UR
WR AA 0 - 2*QC
QQ /AA
RE SOC(I)/(F*AA)
Q(I) Q(I)
P(I) 0.
C(I) 0.
R(I) 0.
A*AMAX1(ABS(U),ABS(V),ABS(W))
FU(I) F*U ABS(V)
FV(I) F*ABS(W)
FW(I) F*ABS(W)
IF (QA(I)*LE.1)*GC TC 42
NS UP NSUP +1
F(I) A*(I+1)
F*U*U -1./QA(I)
FV(I) F*V*V
FW(W) F*W*W
GX X G(I,I+1,J+2) -G(I,J+2) +G(I,J+1,J+2)
GY Y G(I,J+1,J+2) -G(I,J+2) +G(I,J+1,J+2)
GZ Z G(I,I+1,J+1,J+2) -G(I,J+1,J+2) +G(I,J+1,J+2)
GX Y G(I,I+1,J+1,J+2) -G(I,J+1,J+2) +G(I,J+1,J+2)
1 GY Z G(I,I+1,J+1,J+3) -G(I,J+1,J+3) -GL(I,J+1,J+1,J+2)
GZ X G(I,I+1,J+1,J+3) -G(I,J+1,J+3) -GL(I,J+1,J+1,J+2)
FX Y F*25*F
FY Z F*25*V*GXY
FZ X F*25*W*GYZ
P(I) F*W*U*GZX
G(I) FUU(I)*GXX
R(I) FVV(I)*GYY
C(I) FWW(I)*GZZ
4.2 CONTINUE
PF P(2)
DO 52 I=2,NX = -P(2)
AV = RESC(I)*RV
PB = PF
PF = P(I)
IF ((FU(I)+LI*0.)*UP(I-1)) PF = -P(I+1)
A = UP(I) -UP(I-1) +UM(I) +VM(I-1)
1 +VP(I) +VP(I-1) -VP(I) -VM(I-1)

```


JRES

62 AG = KAG +AES(CC(I))
IF (ABS(CC(I))>=CG(I)) GO TO 62
DG = CG(I)

KG = JG

KG = I

I DO 72 I=1,Nx

CGP(I) = QM(I)

DP(I) = FM(I)

FP(I) = VM(I)

UP(I) = WM(I)

WP(I) = AM(I)

BP(I) = BM(I)

CP(I) = CM(I)

ABP(I) = ABM(I)

BCP(I) = BCM(I)

CAP(I) = CAM(I)

ABC(I) = ABCM(I)

72 ABCP(I) = ABCP(I+1)

J IF (J - KY) = 21 E2(K)

12 IF (I TE2(K) .EQ. NX) I2 = NX

IF (ISYN*EQ.1)

DO 82 I=1,NX

IF (IV(I,K) .EQ. EC.1)

IF (IV(I,K) .EQ. 2*OR.IV(I+1,K) .EQ. 2)

M CGK(I) = NX +1

CGK(I) = QQP(M)

DM(I) = DP(I)

FM(I) = UP(I)

VM(I) = WP(I)

AM(I) = BP(I)

BW(I) = CP(I)

CM(I) = ABP(I)

ABM(I) = ABCP(M)

BCM(I) = ABCP(M)

CAM(I) = ABCP(M)

ABC(I) = ABCP(M)

GO TO 82

CGK(I) = DP(I)

82


```

FM(I)
UM(I)
WM(I)
AM(I)
EM(I)
ABM(I)
BCM(I)
CAM(I)
ABCN(I)
CONTINUE
DO 92 I=1,NX
IF (IAES(I,J,K).GT.1) GO TO 92
RE SO(I)=0.
A=-ABP(I)
B=-BCF(I)
C=CAP(I)
D=-ABC(I)
92 CONTINUE
IF (AES(I,J,K).GT.1) GO TO 92
RE SO(I)=0.
A=-AMAX(0,1*ABS(IV(I,K)))
S=A*(G(I+1,J+2)-G(I,J+2)-G(I,J-1,2)+G(I,J-1,J+2))
1 RESL(I,J)
AL(I,J)=S
BL(I,J)=0.
CL(I,J)=0.
S2 CONTINUE
GO TO 41
101 S1 = 5*SCALL(K)
I1 = NX+2
J1 = ITEJ(K)
N1 = NV
IF (I.EQ.I1.OR.I1.EQ.1) GO TO 103
Y1=G(I2,KY,2)
NV1=NV+1
VORT(NV)=VORT(NV)+P3*(V-VORT(NV))
N1 = NV
I1 = 1
V1=0.
IF (IV(I,K).NE.0) GC=TC109
Z2=ZA(K)-TVAW*(X0(K))
GO TO 107
105 N1 = N-1
GO TO 105
103 I1 = -1
V1=0.
IF (IV(I,K).NE.0) GC=TC109
Z2=ZA(K)-TVAW*(X0(K))
GO TO 107
107 A = (Z-ZV(N-1))/(ZV(N)-ZV(N-1))
V1=A*VGRT(N)
M = NX+2
I1 = -1.
106 M = G(M,KY-1,2)
G(M,KY+1,2) = G(I,KY-1,2)
G(M,KY+2) = G(I,KY+2)
IF (I.GT.1) GO TO 103
G(I,KY,2) = -5*V

```



```
G(P,KY,Z)
G(LX,KY+1,2) = *5*V
RETURN
END
```


$\begin{aligned}
& Y(I,J) \\
& Z(I,J) \\
& X(I,J) \\
& YR(I,J) \\
& ZR(I,J) \\
& IF (FUS*LE .0.) GC TC 21 \\
& DO 14 J=1,NX \\
& DO 14 J=1,NX \\
& A = 2.5*(ZR(I,J)**2 - YR(I,J)**2) + FS**2 \\
& B = 5*ZR(I,J)*YR(I,J) \\
& S = SQRT(A**2 + B**2) \\
& T = 0 \\
& IF (S .GT. 0.) T = 5*ATAN2(B,A) \\
& IF (B .EQ. 0.) AND (YR(I,J) .LT. 0) T = .5*PI \\
& IF (B .EQ. C) AND (SQR(T(S)) .LT. 0) T = -.5*PI \\
& SQR(T(S)) \\
& YR(I,J) = .5*S*SIN(T) \\
& ZR(I,J) = .5*S*COS(T) \\
& IF (N.LE.K) GO TO 11 \\
& J = 2, NX + 1 \\
& DO 22 I=2,NX \\
& U = 0. \\
& V = 0. \\
& W = 1 \\
& X = 1 \\
& Y = 1 \\
& Z = 1 \\
& G(1,1,1) = X(I,1,1) - X(I,1,1) \\
& G(1,1,2) = X(I,1,2) - X(I,1,2) \\
& G(1,2,1) = X(I,2,1) - X(I,2,1) \\
& G(1,2,2) = X(I,2,2) - X(I,2,2) \\
& G(1,1,1) = Y(I,1,1) - Y(I,1,1) \\
& G(1,1,2) = Y(I,1,2) - Y(I,1,2) \\
& G(1,2,1) = Y(I,2,1) - Y(I,2,1) \\
& G(1,2,2) = Y(I,2,2) - Y(I,2,2) \\
& G(1,1,1) = Z(I,1,1) - Z(I,1,1) \\
& G(1,1,2) = Z(I,1,2) - Z(I,1,2) \\
& G(1,2,1) = Z(I,2,1) - Z(I,2,1) \\
& G(1,2,2) = Z(I,2,2) - Z(I,2,2) \\
& G(1,1,1) = G(I,J,1) - G(I,J,1) \\
& G(1,1,2) = G(I,J,2) - G(I,J,2) \\
& G(1,2,1) = G(I,J,3) - G(I,J,3) \\
& G(1,2,2) = G(I,J,4) - G(I,J,4) \\
& FXX = -Y*Z*ZY \\
& FYX = -Y*ZX*ZY \\
& FXY = -Y*ZY*ZX \\
& FYZ = -Y*ZX*ZY \\
& FZX = -Y*ZY*ZX \\
& FYY = -Y*ZX*ZY \\
& FYZ = -Y*ZY*ZX \\
& FZY = -Y*ZX*ZY \\
& FZZ = -Y*ZY*ZX \\
& FZ = 1. / (FX*X*XX + FY*X*YY + FZ*X*ZZ)
\end{aligned}$


```

U = U + (FXX*GX + FYX*GY + FZX*GZ) * F + CA
V = V + (FYX*GX + FYY*GY + FZY*GZ) * F + SA
W = W + (FXZ*GX + FYZ*GY + FZZ*GZ) * F + SYAW

IF (M.EC.2) GO TO 25
      X = X(I,1) - X(I-1,1)
      Y = Y(I,1) - Y(I-1,1)
      Z = Z(I,1) - Z(I-1,1)
      G = G(I,J,2) - G(I-1,J,2)

GO TO 25
      N = N.EC.NWPX / GO TO 27
      X = X(I+1,1) - X(I,1)
      Y = Y(I+1,1) - Y(I,1)
      Z = Z(I+1,1) - Z(I,1)
      G = G(I+1,J,2) - G(I,J,2)
      G = G(I,J,2) - G(I,J,1)*2

25 GO TO 27
      U = AV*L
      V = AV*V
      W = AV*W

27 U = V
      V = W
      W = U

      Q = SQR(T(Q))
      A = MACH*SQRT(Q)
      S = T1*(Q**3.5**-1.0)
      C = SCAL(KTE1)*X(I,1)
      P = SCAL(KTE1)*Y(I,1)
      I = SITE1(K)
      E = SITE2(K)
      XMAX = ISCAL(KTE1)*X(I1,1)
      XMIN = XMAX
      YMAX = SCAL(KTE1)*Y(I1,1)
      YMIN = YMAX

DO 22 I=I1,12
      XMAX = AMAX(XMAX,XP(I))
      XMIN = AMIN(XMIN,XP(I))
      YMAX = AMAX(YMAX,YP(I))
      YMIN = AMIN(YMIN,YP(I))

22 RETURN
END

```



```

C***SUBROUTINE CPLCT*****SUBROUTINE CPLCT (13,14,FMACH,XP,YP,C,P,SM,11,12,KPLOT)
C
C PLCTS CF AT COMPUTATIONAL MESH*PCINTS
COMMON /PCKR/ PTK
COMMON /PARMT3/ XT3(161),YT3(161),ZT3(161),
1 COMMON /UVW/ UU(161),VV(161),WW(161),
COMMON /PRS/ XC(161),
COMMON /STARE/ LINE(90),DUMY(10),
DIMENSION KODE(2),XP(1),YP(1),CP(1),SM(1),
DATA IS1/1H/,IH+/,
NOI = C
IMIN = 11 + (12 - 11)/2
CHD = XF(11) - XP(11)/IMIN
2 FORMAT(4OF CP AT COMPUTATIONAL MESH POINTS/
1 ICH0 X * 1CH Y * 1CH 7HMACH NO. 8H CP ,
2 7H XCC * 2X 5+CP * *F8*4*2X, 7HCFGRD =*F1C*4)
CP C = ((1. + .2*FMACH**2)*3.5 -1.)/(.7*FMACH**2)
DO 12 I=1,90
12 LINE(I) = KODE(1)
CPS = (((5. + FMACH**2)/6.)**3 * 5 - 1.)/(.7*FMACH**2)
IF (KPLOT.EQ.0 .OR. KPL0T.GT.15) 15
15 WRITE(6,21) CPS,CHD
KS = 3C.*((CPO - CPS) + 4*5
IF (KS .GE. 1 .AND. KS.LE.90) LINE(KS)=IST
DO 22 I=13,14
22 K = 30.**(CFO - CP(1)) + 4*5
CONTINUE
LINE(K) = MNC(9C,K)
LINE(K) = KODE(2)
XOC = (XF(1) - XP(IN)) / CHD
XOD = (1) = XCC
IF (KPLCT.EQ.0 .OR. KPL0T.GT.1) GC(TC,20)
WRITE(6,(6,610) XP(i),YP(i),SM(i),CP(i),XCC,LINE
20 CONTINUE
LINE(K) = KCODE(1)
IF (I.LT.11.OR.I.GT.12) GO TO 22
NOI = AC1 + 1
XT3(NOI) = XP(1)
YT3(NOI) = YP(1)
ZT3(NOI) = ZU(1)
UT3(NOI) = VV(1)
WT3(NOI) = WW(1)
22 IF (K.EC.KS) LINE(KS)=IST
IF (KPLCT.EC.0 .OR. KPL0T.GT.1) GO TO 25
CALL INCRT6

```


25 CONTINUE
61C RETURN
61C FORMAT (2F10.4,F7.4,F8.4,F7.4,F8.4)
61C ENC


```

C** SUBROUTINE INVRT6 *****
SUBROUTINE INVR16
COMMON /FCCKR/ F7CK
COMMON /PARMT3/ XT3(161), YT3(161), VT3(161), ZT3(161),
1 DIMENSION P(161,61), TEMP(161),
EQUIVALENCE (XT3(1),P(1,1)),
DO 30 I=1,6
DO 10 J=1,NCI
M=N0I-I+1
TEMP(M)=P(I,J)
10 C CONTINUE
DO 20 I=1,NCI
P(I,J)=TEMP(I),
20 C CONTINUE
30 C CONTINUE
WRITE(6,100) (1,XT3(I),I=1,N0I),YT3(1),VT3(1),
1 W13(1),VT3(1),ZT3(1),UT3(1),
1 RETURN
10C FORMAT (4HO 1 ,1X,6HXT3(1),4X,6HZT3(1),4X,6HYT3(1),4X,6HT3(1),
1      4X,6HWT3(1),4X,6HVT3(1),4X,6HZT3(1),4X,6HYT3(1),4X,6HT3(1),
2      6X,4L 1 ,1X,6HXT3(1),4X,6HZT3(1),4X,6HYT3(1),4X,6HT3(1),
3      4X,6HWT3(1),4X,6HVT3(1),4X,6HZT3(1),4X,6HYT3(1),4X,6HT3(1),
4      (14,1X,6G10.3,2X,14,1X,6G10.3))
END

```



```

C**SUBROUTINE FCRCF*****
C   SUBROUTINE FORCF (I1,I2,XP,YP,CP,AL,CHORD,XM,YM,CL,CD,CM)
C   CALCULATES SECTION FORCE EFFICIENCIES
C   DIMENSION = 57; 295779513082
C   RAD = AL/RAD
C   ALPHA = 0.
C   CL = 0.
C   CD = 0.
C   CM = 0.
C   DD = 12  I=11,1,-1
C   DX = ((XP(I+1)) - XP(I))/CHORD
C   DY = ((YP(I+1)) - YP(I))/CHORD
C   XA = 0.5*((XF(I+1) + XP(I)) - XM)/CHORD
C   YA = 0.5*((YF(I+1) + YP(I)) - YM)/CHORD
C   CPA = 0.5*(CP(I+1) + CP(I))
C   DCL = CPA*DX
C   DCE = CPA*DY
C   CL = CL + DCL
C   CD = CD + DCE
C   12 CM = CL*COS(ALPHA) - DCL*SIN(ALPHA)
C   CD = CL*SIN(ALPHA) + DCL*COS(ALPHA)
C   CL = DCL
C   RETURN
C   END

```



```

C***SUBROUTINE TCTFOR***TOTAL FORCE COMPUTATION
      SUBROUTINE TOTFOR (KTE1,KTE2,CHORD,SCL,SCD,SCM,XO,YO,ZPO,
     1 CALCULATES TOTAL FORCE COEFFICIENTS
     2           CHORD(1),SCL(1),SCM(1),X(1),Y(1),ZPO(1)
     3           = ZPO(KTE1)
     4           = 0.
     5           = 0.
     6           = 0.
     7           = 0.
     8           = 0.
     9           = 0.
    10           = KTE1
    11           = SCL(K)*CHORD(K)
    12           = SCD(K)*CHORD(K)
    13           = CHGRD(K)*(SCM(K)*CHORD(K)
    14           = -SCL(K)*X0(K) + SCD(K)*YPO(K))
    15           = 5*(ZPO(K+1) - ZPO(K))
    16           = SC(L(K+1)*CHORD(K+1)
    17           = SCD(K+1)*CHORD(K+1)
    18           = CHORD(K+1)*(SCM(K+1)*CHORD(K+1)
    19           = -SCL(K+1)*X0(K+1) + SCD(K+1)*YPO(K+1)
    20           = DZ*(PL + CL)
    21           = DZ*(PD + QD)
    22           = CL + CLA
    23           = CD + CDA
    24           = CMP + DZ*(PM + QM)
    25           = CMR + AZ*CLA
    26           = CMY + AZ*CLA
    27           = SPL + DZ*(CHORD(K+1) + CHORD(K))
    28           = PD
    29           = PM
    30           = K + 1
    31           = (K+1)*KTE2
    32           = CL/S
    33           = CD/S
    34           = CMP*SPAN/S**2
    35           = (CMR + CMR)/(CMY + CMY)
    36           = RETURN
    37           = END

```



```

C*** SUBROUTINE REFINER
SUBROUTINE REFINER(REFINER,HALVES,SIZE)
COMMON /161/ 18,3,SO(161),35,VORT(115),ZV(115),
1      /161/ 25,ITE1(35),TE2(35),
2      AO(161),B0(18),X0(35),Y0(35),Z0(35),SCAL(35),
3      NX,NY,NZ,KTE1,KTE2,ISY,KSY,FUS,
4      YAW,CYAW,SYAW,ALPHA,CA,SA,FACH,N1,N2,N3,I0
      NX+1,NY+1,NZ+3,NX+2,NY+2,NZ+1,NX+1,NY+1,NZ+2,NY+2,NZ+1
      KY,MY,MZ,O,MYC,MZ,O,K=1
      IF (KSYN.EQ.0) GO TO 11
      MZ,O=NZ/2+3
      READ (N1,ERR=401) ((G(I,J,1),I=1,MX0),J=1,MY0)
      K=2
      IF (KSYN.EQ.0) GO TO 11
      MZ,O=NZ/2+3
      READ (N1,ERR=401) ((G(I,J,1),I=1,MX0),J=1,MY0)
11     READ (N1,ERR=401) ((G(I,J,1),I=1,MX0),J=1,MY0)
      JJ=NY/2+1,KY=MX0
      21   I,I=G(I,I,JJ,1)=G(I,J,1)
      I,I=I,I=-1,-2
      IF (I.GT.0) GO TO 31
      J,J=J,J=-1
      IF (J.GT.0) GO TO 21
      J,J=J,J=-2
      IF (J.GT.0) GO TO 21
      DO 42 J=1,NY,2
      DO 42 I=1,NX,2
      G(I,J,1)=.5*(G(I+1,J,1)+G(I-1,J,1))
      DO 54 I=1,NX,2
      DO 54 J=1,NY,2
      G(I,J,1)=.5*(G(I,J+1,1)+G(I,J-1,1))
      54 G(I,NY,1)=0.
      G(NX2,N1)=0.
      WRITE (N2)((G(I,J,1),I=1,MX),J=1,MY)
      K=K+1
      IF (K.LE.MZC) GO TO 11
      REWIND N1
      REWIND N2
      READ (N2,ERR=401) ((G(I,J,1),I=1,MX),J=1,MY)
      READ (N2,ERR=401) ((G(I,J,1),I=1,MX),J=1,MY)

```



```

K = 1
IF (KSYR•NE•0) K = 2
 111 DO 112 I=1,MY
    DO 112 J=1,MX
      DO 112 I=1,MX
        DO 112 J=1,MY
          G(1,I,J,2) = 5*(G(1,J,1) + G(1,J,3))
        DO 112 J=2,MY
          WRITE (N1) ((G(1,J,M),I=1,MX),J=1,MY)
      112 CONTINUE
      112 IF (K•EC•MXZC) GC TC 201
      DO 112 J=1,MY
        DO 112 I=1,MX
          G(1,I,J,1) = G(1,J,3)
        REAC(N1,ERR=401) ((G(I,J,3),(G(I,J,3),I=1,MX),J=1,MY))
      GO TO 111
    REWIND N1
  201 REWIND N2
    DO 202 I=1,3
      REAC(N1,ERR=401) ((G(I,J,M),I=1,MX),J=1,MY)
  202 CONTINUE
  202 WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MY)
    YAW = SYAH/CYAW
    NV = KTE1 - 1
    VORT(NV) = 0.
  K = 2
  IF (KSYR•NE•0) GO TC 251
  S1 = NV
  211 IF (K•LT•KTE1•QR•K•GT•KTE2) GO TO 231
    IF (K•LT•KTE1•ITE1(K)
    I1 = MX0 + 1
    I1 = ITE1(K)
    I2 = ITET2(K)
    DO 212 I=1,12
      DO 212 J=1,12
        G(I,KY+1,J,2) = G(I,KY,2) + G(I,KY,2) - G(I,KY,2)
      NV = NV + 1
      VORT(NV) = G(I2,KY,2) - G(I1,KY,2)
    NV = NV + 1
    212 IF (K•NF•KTE2•QF•YAW•LE•0.) GO TO 231
      M = NV
      NV = NV + 1
      VORT(NV) = G(M,KY,2) - G(I,KY,2)
    IF (I•LT•MX0) GC TD 221
      I = 1
      I = 0.
  231 I = 1
      V = 0.

```



```

IF (IV(I,K)*NE(1)) GO TO 237
233 IF (ZL*EE.ZV(N-1)) -TYAW*(X0(K) + S1*AC(I)*A0(I))
      N = N-1
      GO TO 233
235 A = ((ZV(N-1))/(1.-A))*VCFI(N-1)
      V = NX+2 -I
      G(I,KY+1,2) = G(M,KY-1,2) -V
      G(M,KY+1,2) = G(I,KY-1,2) +V
      IF (IV(I,K)+1).NE.0.5*G(I,KY,1) +.25*(G(I,KY,3)
      G(I,KY,(I+1)*LT1) = G(I,KY,3) +.25*(G(I,KY,1)
      1G(I,KY,2) = G(I,KY,2) +G(M,KY,2)
      G(I,KY-1,2) = 0.5*(G(M,KY,2)
      G(I,KY-1,2) = 0.5*(G(M,KY-2,2)
      G(I,KY,2) = -0.5*V
231 IF (I*G1*1) GO TO 231
      G(I,KY,2) = 0.5*V
      K = K+1
      IF (K*EG.MZ) GO TO 261
      DO 252 J=1,MY
      DO 252 J=1,MY
      G(I,J,1) = G(I,J,2)
      G(I,J,2) = G(I,J,3)
      WRITE (N2,ERR=401) ((G(I,J,I=1,MX),J=1,MY),
      READ (N1,ERR=401) ((G(I,J,J=1,MX),J=1,MY)
      GO TO N2
      261 VORT(N2) = 0.
      DO 262 I=2,M
      WRITE (N2,((G(I,J,M),I=1,MX),J=1,MY)
      262 CONTINUE
      262 REWIND N1
      DO 302 K=1,MZ
      REAC(N2,ERR=401,((G(I,J,I=1,MX),I=1,MX),J=1,MY))
      WRITE (N1,((G(I,J,I=1,MX),I=1,MX),J=1,MY))
      302 CONTINUE = 1
      RETURN = 0
      401 RETURN
      ENC

```



```

C***SUBROUTINE SMCC***SUBROUTINE SMOC
COMMON SMCOTH,FCTEN,AL
      G(161,18,3),S0(161,35),VORT(115),ZV(115),
      IV(161,35),ITE1(35),ITE2(35),
      AO(161),BO(18),X0(35),YC(35),Z0(35),SCAL(35),
      NX,NY,NZ,KTE1,KTE2,ISYM,KSYM,FUS,
      YAW,CYAW,SYAW,ALPHA,CA,SA,FRACTION,N1,N2,N3,I0
      MX,KY,MZ,K1,K2,(KSYM+EC*0) GO TO 1
      K1=NY+1,K2=NZ+2
      K1=NY+1,K2=NZ+3
      IF(K2-NZ+2>0) THEN
      1 PX=1./E6.,PY=1./E6.,PZ=1./E6.
      DO 2 L=1,3
      READ(51,ERR=51) ((G(I,J,L),I=1,MX),J=1,NY)
      2 CONTINUE
      WRITE(62) ((G(I,J,1),I=1,MX),J=1,NY)
      K=K+1
      11 DO 12 J=3,NY
      DO 14 I=1,J,1 = (1.-FX,-PY,-PZ)*G(I+1,J+2)
      14 G(I,J,1) = +.5*PX*(G(I+1,J+2)+G(I-1,J+2))
      .5*PY*(G(I,J+1)+G(I,J-1)) +G(I,J,1)
      +.5*PZ*(G(I,J,3)+G(I,J,1))
      12 G(MX,J,1) = G(MX,J,2)
      DO 16 I=1,NX
      G(I,1,1) = G(I,1,2)
      G(I,1,2) = G(I,1,1)
      G(I,1,KY,1) = G(I,1,KY,2)
      G(I,1,MY,1) = G(I,1,MY,2)
      16 WRITE(62) ((G(I,J,1),I=1,MX),J=1,NY)
      IF((K-EC*K2)>0) GO TO 31
      DO 22 J=1,NY
      DO 22 I=1,NX
      G(I,J,1) = G(I,J,2)
      22 READ(51,ERR=51)((G(I,J,3),I=1,MX),J=I,NY)
      GO TO 31
      WRITE(62) ((G(I,J,3),I=1,MX),J=1,NY)

```



```
REWIND N1
REWIND N2
DO 42 K=1, MZ
READ (N2,ERR=51), ((G(I,J,1), I=1,MX), J=1,MY)
WRITE (N1) ((G(I,J,1), I=1,MX), J=1,MY)
CONTINUE
42 IO RETURN = 1
51 IO RETURN = 0
END
```



```

C** SUBROUTINE SPLIF***SPLIF(N,S,F,FP,FPP,KN,VM,KN,VN,MODE,FQM,IND)
C SPLINE FIT - JAPSEN
C INTEGRAL PLACED IN FPP IF MODE GREATER THAN 0
C INDSECT C ZERO IF DATA IS LEGAL
C DINESIGN = 0 IF (1), F(1),FP(1) ,FPPP(1)
C DINC = 1 IF (K - 1) = E1,81,1
C K = (N - M)/K
1   1   J DS    = N +K      -S(I)
     1   J DS    = S(J) -S(I)
11  DF (DS) 11*81 11
11  DF (KM -2) = {F(J) -F(I)}/CS
12  U V GO TO 25 = 5,13,14
     12  U V GO TO 25 = 3.* (DF -VN)/DS
13  U V GO TO 25 = 0M
14  U V GO TO 25 = -1.5*VM
21  J DS    = J +K      -S(I)
     21  J DS    = S(J) -S(I)
22  DF (D*CS) 81 123
     22  DF = {F(J) -F(I)}/DS
     22  B = B*DS/DS +U
     22  B = B*(C.*DF -V)
25  FP(I), = V(2*-U)*DS
     25  U V = 6.*CF +DS*V
31  IF ({J -N) 21 31 21
     31  IF (KN -2) 32 33 34
     31  V GO TO 25 = (6.*VN -V)/U
32  V GO TO 25 = VN
33  V GO TO 25 = VN
     33  B = V(DS*VN +FPP(I))/(1. +FP(I))
     33  B = DS(J) -S(I)
41  DS

```



```

6 FPPP(I)      = FPP(I) - FF(I)*V
   FPF(I)      = (V-U)/DS
   FP(I)       = U(F(J) - F(I))/DS - DS*(V +L +U)/6.
V   J             = I
   IF (J -N)    = I -K
   = I, 51,41
51  FPP(N)      = N-K
   FPP(N)      = FPP(I)
   FP(N)       = B
   FP(N)      = DF +D*(FPP(I) +B +B)/6.
INC  IF (M0FE)  81'81,61
   FP FP(J)   = FQM
   FP FP(J)   = FQp(J)
71   J             = J
   DS           = S(J) -S(I)
   DS           = FPP(J)
   FPP(J)      = FPP(I) +.5*DS*(F(I) +F(J) -DS*DS*(U +V)/12.)
V   J             = U
   IF (J-N)    71 81 71
   INC(EC-1)  71 81 71 90
81  WRITE((685) INC'MCDE,10^K4/; S(I),S(J),DS,E
85  FORMAT(6HOCHECK610^4G13,I=1,4)
85  WRITE((686)(S(I),F(I),I=M,N)
86  FORMAT(10G13.4)
SC  RETURN
END

```



```

C** SUBROUTINE VERTEC *****
C   SUBROUTINE VERTEC (I1,I2,XCCD,CP,NRD,ZPC,FMACH,YA,AL,
1      SCL,SCD,SCM,K)
C
C   SUBROUTINE FOR VERSATEC PLOTTING OF THE PRESSURE COEFFICIENT
C   VS NON-DIMENSIONAL CHORD (X/C) FOR EACH SECTION OF THE FINAL
C   MESH
C
      REAL PXCC(165), PCP(165), XCL0(85), XCLP(85), CPLO(85),
1      XCUP(85), ZPO(35), SCL(35), SCM(35), SCD(35),
2      INTEGER I,J,NUM,NUM1,II,12,NRD,K
C
C   INITIALIZE ARRAYS AND DATA TO ZERO.
      NUM = C.0
      NUM1 = C.0
      DO 10 I=1,165
         PXCC(I) = 0.0
         PCP(I) = 0.0
10     CONTINUE
      DO 20 J=1,85
         XCLC(J) = 0.0
         CPLC(J) = 0.0
         XCUP(J) = 0.0
         CPUP(J) = 0.0
20     CONTINUE
C
C   READ IN X/C AND CP DATA INTO NEW ARRAY STARTING AT ARRAY
C   ELEMENT NUMBER 1
      DO 30 I=1,12
         PXCC(I-1) +1 = XCUP(I)
         PCP(I-1) +1 = CPUP(I)
30     CONTINUE
      PXC(NRC) = 1.0
C
C   PUT THE DATA INTO TWO ARRAYS ONE FOR THE LOWER SURFACE
C   AND ONE FOR THE UPPER SURFACE
      NUM = (NRD-1)/2
      NUM1 = NRD +1
      DO 40 I=1,NUM1
         XCLC(I) = PXCC(I)
         CPLC(I) = PCP(I)
40     CONTINUE
      DO 50 J=NUM1, NRD
         XCUP(J-NUM) = PXC(J)
         CPUP(J-NUM) = PCP(J)
50     CONTINUE
C
C   INITIALIZE THE VERSATEC PLTTER SYSTEM

```



```

C CALL PLTIS (0, 0, 0, 0)
C SCALE THE DATA TO AN 5.0 X 7.0 INCH SPACE
C CALL SCALE (PXC, 5.0, NRD, +1)
C CALL SCALE (PCP, 7.0, NRD, -1)

C DRAW THE X AND Y AXES
C CALL AXIS (1.0, 2.0, 'X/C', '-3.5, 0.0, C, PXC(NRD+1), PXC(NRD+2))
C CALL AXIS (1.0, 2.0, 'Y/C', '0.0, C, EFFICIENT(CF), 25,
C >7.0, 90, C, PCP(NRD+1), PCP(NRD+2))
C PUT SCALE FACTORS INTO TWO ARRAYS FOR UPPER AND LOWER SURFACE
C XCLC(NRD+1) = PXC(NRD+1)
C XCLC(NRD+2) = PXC(NRD+2)
C CPLC(NRD+1) = PCP(NRD+1)
C CPLC(NRD+2) = PCP(NRD+2)

C XCLP(NRD+1) = PXC(NRD+1)
C XCLP(NRD+2) = PXC(NRD+2)
C CPLP(NRD+1) = PCP(NRD+1)
C CPLP(NRD+2) = PCP(NRD+2)

C PLCT THE DATA POINTS
C CALL NEOPEN (2)
C CALL PLCT (1.0, 2.0, '-3)
C CALL LINE ('XCLP, CPLC, NUM1, 1, -1, 11)
C CALL LINE ('CPLP, NUM1, 1, -1, 11)

C PLACE TITLE AT TOP OF PAGE
C CALL SYNPEN (3)
C CALL SYNPEN (1, 25, 7.5, 0.2, 'SECTION CP DATA', 0.0, 0.16)
C CALL SYNPEN (1)
C CALL SYNPOL (1, 25, 7.0, 0.1, '* = UPPER SURFACE', 0.0, 0.18)
C CALL SYNPOL (1, 25, 7.0, 0.1, '+ = LOWER SURFACE', 0.0, 0.18)

C PLACE FICTITIOUS INFORMATION ON PLOT
C CALL NEOPEN (2)
C CALL SYNPOL (0.0, -75, 0.1, 'SPAN STATION = ', 0.0, 0.15)
C CALL NUMBER (9.9, 0.0, 9.9, 0.0, 1, ZPO(K), C, 0, +1)
C CALL NUMBER (0.0, -1.0, 0.0, 1, MAC, !, 0, 0, +1)
C CALL NUMBER (9.9, 0.0, 9.9, 0.0, 1, FMACH, !, 0, 0, +1)
C CALL NUMBER (2.0, -1.0, 0.0, 1, YAW, !, 0, 0, +1)
C CALL NUMBER (9.9, 0.0, 9.9, 0.0, 1, YAW, 0.0, +3)
C CALL NUMBER (4.0, -1.0, 0.0, 1, AOA, 0.0, +3, 5)
C CALL NUMBER (9.9, 0.0, 9.9, 0.0, 1, AL, 0.0, +3, 5)
C CALL NUMBER (0.0, -1.25, 0.0, 1, CL, 0.0, +3, 6)
C CALL NUMBER (9.9, 0.0, 9.9, 0.0, 1, SCL (K), 0.0, +3)
C CALL NUMBER (2.0, -1.25, 0.0, 1, CD, 0.0, +3)

```



```
CALL NUMBER (995., 999., 0.1, SCD(K), 0.0,+5)
CALL SYBCL (4.0,-1.25,0.1,SCM
CALL NUMBER (995., 999., 0.1, SCM(K), 0.0,+5)
C ENC PLCTTNG
CALL PLCT (0.0,0.0,+999)
RETURN
ENC
```


APPENDIX F

THIS APPENDIX PRESENTS THE SOURCE CODE FOR THE INTERACTIVE PROGRAM FLOW IN

3456112345
 F14VF/-00571•00291•00201•00161•00051•00005•00100•00200•
 •00291•00571•00141•00171•00229•00286•00571•00857•01429;
 •20001•02571•001•03143•03714•04286•04857•05429•06571•0714;
 •88571•01000/•00560•00164•00320•00451•00549•00571•00574•00573;
 •00076•00461•00341•00361•00343•00343•00280•00185•00171•00143•00114;
 -00028•-00037•-00059•-00091•-00115•-00137•-00160•-00160;-00202;
 --00240•-00289•-00343•-00366•-00375•-00375•-00366;-00343;

C*****A-7 WING SECTION - TYPICAL*****
 DATA A7FN/33/0 / A7UM/33/
 A7XF/1 / 00125 / 00075 / 00500 / 00025 / 0015 / 00010 /
 00015 / 0025 / 00500 / 0075 / 00125 / 0025 / 000500 / 00010 /
 00015 / 0025 / 00500 / 0075 / 00125 / 0025 / 000500 / 00010 /
 00015 / 0025 / 00500 / 0075 / 00125 / 0025 / 000500 / 00010 /
 A7VF/ 00000 / 01638 / 03018 / 03500 / 0109 / 02897 / 00900 / 00321 /
 00311 / 01007 / 01468 / 01705 / 01855 / 02030 / 02130 /
 002190 / 02456 / 02650 / 02776 / 02934 / 03018 /
 003137 / 03291 / 03373 / 03390 / 03350 / 02897 / 03309 /
 0023500 / 03018 / 01638 / 00010 /

C*****NACA 0010 AIRFOIL SECTION*****
 DATA N1CFN/37.0/N1CNUN/37/
 N10XP/1.0000,•.9000,•.8000C,•.7000,•.6000C,•.5000,•.4000,•.3000,
 1.2.0000,•.55CC,•.95CC,•.1000,•.1500,•.2000,•.2500,•.3000,•.3500,
 3.0000,•.0500,•.0125,•.0250,•.0500,•.0750,•.1000,•.1250,•.1500,•.2000,
 4.2500,•.3000,•.4000,•.5000,•.6000,•.7000,•.8000,•.9000,•.9500,
 5.1000,•.0105,•.0672,•.01207,•.02187,•.03053,•.03803,•.04412,•.04857,
 1.2.0500,•.04952,•.04585,•.04782,•.04455,•.04985,•.03500,•.03902,•.02962,
 3.01578,•.0000,•.0000,•.0000,•.0000,•.00985,•.01578,•.02178,•.02962,

5

- .03500,-.03902,-.04455,-.02187,-.04952,-.05092,-.04837,
 - .04412,-.03803,-.03053,-.01207,-.00105,

C***** DATA N34FN/45• 0 / N34NUM/45/, 0010-34 SECTION DATA*****
 1 N34XP/1• 0000 • 9500 • 00900 • 08900 • 07000 • 06000 • 05000 • 04000 • 03000 •
 2 0050 • 00205 • 00100 • 00050 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00075 •
 3 00075 • 00100 • 00200 • 00250 • 00300 • 00350 • 00400 • 00450 • 00500 • 00550 •
 4 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 •
 5 N34YF/ 00010 00005 00027 00037 00044 00037 00050 00037 00055 00037 00070 00037 00075 00025 00037 00044 00026 00043 00029 00078 00048 00056,-.
 6 - .03902,-.04455,-.02187,-.04952,-.05092,-.04837,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.

C***** DATA N35FN/45• 0 / N35NUM/45/, 0010-35 SECTION DATA*****
 1 N35XF/1• 0000 • 9500 • 00900 • 08900 • 07000 • 06000 • 05000 • 04000 • 03000 •
 2 0050 • 00205 • 00100 • 00050 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00075 •
 3 00075 • 00100 • 00200 • 00250 • 00300 • 00350 • 00400 • 00450 • 00500 • 00550 •
 4 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 •
 5 N35YF/ 00100 00117 00178 00378 00650 00505 00370 00505 00228 00285 00184 00267 00180 00075 00070 00065 00060 00055 00050 00048 00044 00026 00018 000180,-.
 6 - .03902,-.04455,-.02187,-.04952,-.05092,-.04837,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.

C***** DATA N64FN/45• 0 / N64NUM/45/, 0010-64 SECTION DATA*****
 1 N64XF/1• 0000 • 9500 • 00900 • 08900 • 07000 • 06000 • 05000 • 04000 • 03000 •
 2 0050 • 00205 • 00100 • 00050 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00075 •
 3 00075 • 00100 • 00200 • 00250 • 00300 • 00350 • 00400 • 00450 • 00500 • 00550 •
 4 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 • 00000 •
 5 N64YF/ 00100 00085 00155 00276 00353 00441 00456 00468 00121 00100 00073 00065 00139 00121 00073 00065 00055 00050 00048 00044 00027 00035 00013 00012 00011 00010 00009 00008 00007 00006 00005 00004 00003 00002 00001 00000,-.
 6 - .03902,-.04455,-.02187,-.04952,-.05092,-.04837,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.

C***** DATA N66FN/45• 0 / N66NUM/45/, 0010-66 SECTION DATA*****
 1 N66XF/1• 00000 • 95000 • 009000 • 089000 • 070000 • 060000 • 050000 • 040000 • 030000 •
 - .03902,-.04455,-.02187,-.04952,-.05092,-.04837,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.
 - .03803,-.03053,-.01207,-.00105,-.
 - .04412,-.03803,-.03053,-.01207,-.00105,-.

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6	N63AYF/	75001	80000	85000	90000	95000	100000	030441	035171
1	/	00021	• 00525	• 01030	• 01535	• 02040	• 02545	• 030441	• 035171
2		03943	• 04311	• 04613	• 04837	• 04968	• 04995	• 049131	• 047141
3		• 04405	• 03950	• 03324	• 02917	• 02412	• 01737	• 012501	• 009831
4		• 00815	• 00030	• 00815	• 00983	• 01250	• 01737	• 0141295	• 01241295
5		• 02917	• 03241	• 03950	• 04400	• 04714	• 04943	• 049413	• 049951
6		• 04968	• 04837	• 04613	• 04311	• 02917	• 02412	• 035471	• 030441
7		-02545	-02040	-01535	-01030	-00525	-00021		

N650YF/. 7500 • 8000 • 8500 • 9000 • 9500 • 1000 • 02584 • 03156 • 03682,
 . 0000 • 0030 • 0060 • 0081 • 01385 • 01987 • 02584 • 03156 • 03682,
 . 04146 • 04530 • 04812 • 04963 • 04996 • 04924 • 04760 • 04503,
 . 04143 • 03666 • 03C40 • 02647 • 02177 • 01574 • 01169 • 00932,
 . 002672 • 0.0001 • 0.0072 • 0.0052 • 0.00165 • 0.01574 • 0.02177,
 . 002647 • -0.03040 • -0.03666 • -0.04143 • -0.04503 • -0.04760 • -0.04924,
 . 004996 • -0.04963 • -0.04812 • -0.04536 • -0.04146 • -0.03682 • -0.03156,
 . -0.02584 • -0.01987 • -0.01385 • -0.00810 • -0.00306 • 0.00/

```
C-- FILE DEFINITIONS
C-- CALL FRIGMS ('FILEDEF ''5      ','TERM   ')
C--          ('FILEDEF ''8      ','DISK   ')
C--          ('DATAIN  '1      ','FL027   ')
C--
```


C-- TITLE PAGE AND INSTRUCTIONS

```

CALL FRICMS ('CLRSCRN ')
WRITE (6,410)
WRITE (6,410)
WRITE (6,420)
WRITE (6,430)
WRITE (6,410)
WRITE (6,410)
WRITE (6,440)
WRITE (6,410)

C-- FIRST LINE INPUT DATA--DEFINE COMPUTATIONAL GRID
C-- CONTINUE
C-- WRITE (6,450)
C-- READ (5,1000) TITLE
      10  CONTINUE
      WRITE (6,470)
      READ (5,*)
      WRITE (6,480)
      READ (5,*)
      WRITE (6,490)
      READ (5,*)
      WRITE (6,490)
      READ (5,*)
      CALL FRICMS ('CLRSCRN ')
      WRITE (6,500)
      READ (5,*)
      WRITE (6,510)
      READ (5,*)
      PLOT
      READ (5,*)

C-- SUMMARY OF FIRST LINE INPUT DATA
C-- CONTINUE
C-- CALL FRICMS ('CLRSCRN ')
C-- WRITE (6,520)
C-- READ (5,*)
      ANS
      IF (ANS .GE. 2) GO TO 20
      WRITE (6,521)
      WRITE (6,522)
      FNX, FNY, FMESH, FPLG1
      WRITE (6,530)
      REAL (5,*)
      ANS
      IF (ANS .EQ. 1) GO TO 10
      20  CONTINUE

C-- SECOND, THIRD AND FORTH LINES INPUT DATA--ITERATION AND CONVERGENCE
C-- TOLERANCE FOR GRID. NUMBER OF LINES ECALL 10 M = FMESH
      M = IFIX(FMESH)
      CALL FRICMS ('CLRSCRN ')

```



```

      WRITE (6,450)
      DO 30 I=1,N
        WRITE (1,EC0, 1) WRITE (6,541)
        IF (1,EC0, 2) WRITE (6,542)
        IF (1,EC0, 3) WRITE (6,543)
        WRITE (5,*)
        WRITE (5,550) FIT(1)
        READ (5,*)
        WRITE (5,560)
        WRITE (5,*)
        WRITE (5,570) COVO(1)
        READ (5,*)
        WRITE (5,580) P10(1)
        CALL FRICMS ('CLRS CRN ')
30    CONTINUE

C-----SUMMARY OF SECOND, THIRD AND FORTH LINES INPUT DATA-----
C-----CALL FRICMS ('CLRS CRN ')
      WRITE (6,580)
      READ (5,*)
      IF (ANS*GE*2) ANS
      WRITE (6,581)
      WRITE (6,582) (FIT(I),COVO(I),P10(I)),I=1,M)
      WRITE (6,590)
      READ (5,*)
      IF (ANS.EQ.1) ANS
      READ (5,*)
      IF (ANS.EQ.1) GO TO 20
40    CONTINUE

C-----FIFTH LINE INPUT DATA--MACH NO., YAW ANGLE, AOA, SKIN FRICTION DRAG-----
C-----CALL FRICMS ('CLRS CRN ')
      WRITE (6,450)
      WRITE (6,600)
      READ (5,*)
      WRITE (6,610) FMACH
      READ (5,*)
      WRITE (6,620) YA
      READ (5,*)
      WRITE (6,620) AL
      WRITE (6,630)
      READ (5,*)
      CDO

C-----SUMMARY OF FIFTH LINE INPUT DATA-----
C-----CALL FRICMS ('CLRS CRN ')
      WRITE (6,640)
      READ (5,*)
      IF (ANS*GE*2) ANS
      WRITE (6,641)
      WRITE (6,642) FMACH,YA,AL,CDO

```



```

      WRITE (6,650)
      READ (5,*),ANS
      IF (ANS.EQ.1) GO TO 40
      CONTINUE
C-----SIXTH LINE INPUT DATA--WING PLANFORM SYMMETRY, NUMBER OF SECTIONS,
C-----SWEEP, DIHEDRAL ANGLE AND FUSELAGE RADIUS
C-----CALL FRICMS (' CLRS CRN ')
      WRITE (6,450)
      WRITE (6,60)
      READ (5,*),ZSYM
      WRITE (5,*),CN
      READ (5,*),FNS
      WRITE (5,*),D
      READ (5,*),SWEEP
      WRITE (5,*),90
      READ (5,*),DIHED
      WRITE (5,*),700
      WRITE (5,*),FUS
C-----SUMMARY OF SIXTH LINE INPUT DATA
C-----CALL FRICMS (' CLRS CRN ')
      WRITE (6,710)
      READ (5,*),ANS
      IF (ANS.GE.2) GO TO 60
      WRITE (6,711)
      WRITE (6,712) ZSYM,FNS,SWEEP,DIHED,FUS
      WRITE (6,720)
      READ (5,*),ANS
      IF (ANS.EQ.1) GO TO 50
      CONTINUE
C-----WRITE JCL CARDS TO TOP OF FILE ON USER'S "A" DISK
C-----WRITE (6,120)
      WRITE (6,120)
      WRITE (6,120)
C-----WRITE FIRST SIX LINES OF DATA TO FILE ON USER'S "A" DISK
C-----WRITE (6,1010) TITLE
      WRITE (6,1010)
      WRITE (6,1020)
      WRITE (6,1020)
      WRITE (6,1040)
      WRITE (6,1040)
      WRITE (6,1050)
      WRITE (6,1050)
      WRITE (6,1060)
      WRITE (6,1060)
      WRITE (6,1070) FMACH,YA,AL,CDO

```



```
WRITE (6,1080) ZSYM,FNS,SWEET,DIHEL,FUS
C-----SECTION INFLT DATA-----C
C-----
```

```
N = IFIX(FNS) • CLRS CRN •
```

```
CALL FR7CM5
```

```
WRITE (6,45C)
```

```
WRITE (6,730)
```

```
WRITE (6,410)
```

```
DO 200 I=1,N
```

```
WRITE (6,760) 1
```

```
WRITE (6,770)
```

```
READ (5,*),ZS
```

```
READ (5,*),XL
```

```
READ (5,*),YL
```

```
READ (5,*),YL
```

```
READ (5,*),GRD
```

```
READ (5,*),THICK
```

```
READ (5,*),AI
```

```
READ (5,*),AT
```

```
CALL FR7CM5 ('CLRS CRN')
```

```
WRITE (6,830) FSEC
```

```
READ (5,*),FSEC
```

```
WRITE (6,1100)
```

```
IF (FSEC .EQ. 0.0) GO TO 190
```

```
CALL FR7CM5 ('CLRS CRN')
```

```
WRITE (6,450)
```

```
WRITE (6,740)
```

```
WRITE (6,750)
```

```
REAL (5,*),ANS
```

```
FLAG = ANS
```

```
IF (FLAG .GT. 0) GO TO 70
```

```
WRITE (6,840)
```

```
READ (5,*),YSYM
```

```
CALL FR7CM5 ('CLRS CRN')
```

```
WRITE (6,850)
```

```
REAL (5,*),FN
```

```
C-----USER INPUT X AND Y COORDINATES FOR WING SECTION DEFINING GEOMETRY-----C
C-----
```

```
NUM = IFIX(FN)
CALL FR7CM5 ('CLRS CRN')
```



```

180      WRITE(6,450) 1
        WRITE(6,860) 1
        DO 180 J=1,NUM
        WRITE(5,470) XP(J),YP(J)
        READ(5,470) XP(J),YP(J)
        CONTINUE
        IF (YSYM .EQ. 0.0) GC TC 185
        N1 = NUM + NUM
        J1 = NUM
        DO 182 IA=1, J1
        XF(N1-IA) = XP(IA)
        YF(N1-IA) = -YP(IA)
        CONTINUE
        NUM = FN + (FN - 1.0)
        FN = FN -
        CONTINUE
        WRITE(8,1120) FN
        WRITE(8,1130) FN
        WRITE(8,1140)
        WRITE(8,1150) ((XP(J),YP(J)),.
        GO TO 190
        CONTINUE

183      C-----C MENU INPUT X AND Y COORDINATES FOR W
        C-----C
        IF (FLAG .EQ. 1) GO TO 81
        IF (FLAG .EQ. 2) GO TO 83
        IF (FLAG .EQ. 3) GO TO 84
        IF (FLAG .EQ. 4) GO TO 85
        IF (FLAG .EQ. 5) GO TO 86
        IF (FLAG .EQ. 6) GO TO 87
        IF (FLAG .EQ. 7) GO TO 88
        IF (FLAG .EQ. 8) GO TO 89
        IF (FLAG .EQ. 9) GO TO 90
        IF (FLAG .EQ. 10) GO TO 91
        IF (FLAG .EQ. 11) GO TO 92
        IF (FLAG .EQ. 12) GO TO 93
        IF (FLAG .EQ. 13) GO TO 94
        IF (FLAG .EQ. 14) GO TO 95
        IF (FLAG .EQ. 15) GO TO 96
        IF (FLAG .EQ. 16) GO TO 97
        IF (FLAG .EQ. 17) GO TO 98
        IF (FLAG .EQ. 18) GO TO 99
        IF (FLAG .EQ. 19) GO TO 100
        IF (FLAG .EQ. 20) GO TO 101
        CCNTINUE
        WRITE(8,1120) FP FN

```


82

WKRITETO190 ((FPXP(J),FPYP(J)),J=1,FPRNUM)

CCNNTTINUE((8,1120) SYMFN

CCNRTTE((8,1140) ((SYMXP(J),SYMP(J)),J=1,SYMMUM)

CCNRTTINUE((8,1120) SCHFN

CCNRTTE((8,1130) ((SCWXP(J),SCHYP(J)),J=1,SCWNUM)

CCNRTTINUE((8,1120) N572FN

CCNRTTE((8,1130) ((N572XP(J),N572YP(J)),J=1,N57NUM)

CCNRTTINUE((8,1140) ((N572XP(J),N572YP(J)),J=1,N57NUM)

CCNRTTINUE((8,1150) ((N572XP(J),N572YP(J)),J=1,N57NUM)

83

CCNRTTINUE((8,1120) A7FN

CCNRTTINUE((8,1130) ((A7XP(J),A7YP(J)),J=1,A7NUM)

CCNRTTINUE((8,1140) ((A7XP(J),A7YP(J)),J=1,A7NUM)

CCNRTTINUE((8,1150) ((A7XP(J),A7YP(J)),J=1,A7NUM)

84

CCNRTTINUE((8,1120) LISFN

CCNRTTINUE((8,1130) ((LISXP(J),LISYP(J)),J=1,LISNUM)

CCNRTTINUE((8,1140) ((LISXP(J),LISYP(J)),J=1,LISNUM)

CCNRTTINUE((8,1150) ((LISXP(J),LISYP(J)),J=1,LISNUM)

85

CCNRTTINUE((8,1120) N1CFN

CCNRTTINUE((8,1130) ((N10XP(J),N10YP(J)),J=1,N10NUM)

CCNRTTINUE((8,1140) ((N10XP(J),N10YP(J)),J=1,N10NUM)

CCNRTTINUE((8,1150) ((N10XP(J),N10YP(J)),J=1,N10NUM)

86

CCNRTTINUE((8,1120) N34FN

CCNRTTINUE((8,1130) ((N34XP(J),N34YP(J)),J=1,N34NUM)

CCNRTTINUE((8,1140) ((N34XP(J),N34YP(J)),J=1,N34NUM)

CCNRTTINUE((8,1150) ((N34XP(J),N34YP(J)),J=1,N34NUM)

87

CCNRTTINUE((8,1120) N34FN

CCNRTTINUE((8,1130) ((N34XP(J),N34YP(J)),J=1,N34NUM)

CCNRTTINUE((8,1140) ((N34XP(J),N34YP(J)),J=1,N34NUM)

CCNRTTINUE((8,1150) ((N34XP(J),N34YP(J)),J=1,N34NUM)

88

CCNRTTINUE((8,1120) N34FN

CCNRTTINUE((8,1130) ((N34XP(J),N34YP(J)),J=1,N34NUM)

CCNRTTINUE((8,1140) ((N34XP(J),N34YP(J)),J=1,N34NUM)

CCNRTTINUE((8,1150) ((N34XP(J),N34YP(J)),J=1,N34NUM)

89

90
~~WKRITET(8,1150) ((N34XP(J),N34YP(J)),J=1,N34NUM)~~
~~GCNITINUE~~
~~CCRITET(8,1120)~~
~~WKRITET(8,1130)~~ N35FN
~~WKRITET(8,1140)~~
~~WKRITET(8,1150) ((N35XP(J),N35YP(J)),J=1,N35NUM)~~

 91
~~GCNITINUE(8,1120)~~ N64FN
~~CCRITET(8,1130)~~
~~WKRITET(8,1140)~~
~~WKRITET(8,1150) ((N64XP(J),N64YP(J)),J=1,N64NUM)~~

 92
~~GCNITINUE(8,1120)~~ N66FN
~~CCRITET(8,1130)~~
~~WKRITET(8,1140)~~
~~WKRITET(8,1150) ((N66XP(J),N66YP(J)),J=1,N66NUM)~~

 93
~~GCNITINUE(8,1120)~~ N16FN
~~CCRITET(8,1130)~~
~~WKRITET(8,1140)~~
~~WKRITET(8,1150) ((N16XP(J),N16YP(J)),J=1,N16NUM)~~

 94
~~GCNITINUE(8,1120)~~ N63FN
~~CCRITET(8,1130)~~
~~WKRITET(8,1140)~~
~~WKRITET(8,1150) ((N63XP(J),N63YP(J)),J=1,N63NUM)~~

 95
~~GCNITINUE(8,1120)~~ N63AFN
~~CCRITET(8,1130)~~
~~WKRITET(8,1140)~~
~~WKRITET(8,1150) ((N63AXP(J),N63AYP(J)),J=1,N63AN)~~

 96
~~GCNITINUE(8,1120)~~ N640FN
~~CCRITET(8,1130)~~
~~WKRITET(8,1140)~~
~~WKRITET(8,1150) ((N640XP(J),N640YP(J)),J=1,N640N)~~

 97
~~GCNITINUE(8,1120)~~ N64AFN
~~CCRITET(8,1130)~~


```

      WRITE(8,1140) ((N64AXP(J),N64AYP(J)),J=1,N64AN)
      WRITE(8,1150) ((N64AXP(J),N64AYP(J)),J=1,N64AN)
      CCNTINE
      CCNTINE(8,1120) N650FN
      CCNTINE(8,1130) ((N650XP(J),N650YP(J)),J=1,N650N)
      CCNTINE(8,1140) ((N650XP(J),N650YP(J)),J=1,N650N)
      CCNTINE(8,1150) ((N650XP(J),N650YP(J)),J=1,N650N)

      99      CCNTINE(8,1120) N65AFN
      CCNTINE(8,1130) ((N65AXP(J),N65AYP(J)),J=1,N65AN)
      CCNTINE(8,1140) ((N65AXP(J),N65AYP(J)),J=1,N65AN)
      CCNTINE(8,1150) ((N65AXP(J),N65AYP(J)),J=1,N65AN)

      100     CCNTINE(8,1120) N660FN
      CCNTINE(8,1130) ((N660XP(J),N660YP(J)),J=1,N660N)
      CCNTINE(8,1140) ((N660XP(J),N660YP(J)),J=1,N660N)
      CCNTINE(8,1150) ((N660XP(J),N660YP(J)),J=1,N660N)

      110     CALL FR7CMS('CLRS CRN')
      CONTLE

      C-- WRITE THREE LINES TO USER'S FILE INDICATING END OF CALCUL
      C-- WRITE(8,1160)
      C-- WRITE(8,1170)
      C-- WRITE(8,1180) ZERC

      C-- WRITE JCL CARDS TO BOTTOM OF FILE ON USER'S "A" DISK
      C-- WRITE(8,1220)
      C-- WRITE(8,1230)

      C-- INDICATE TO USER THAT INPUT IS COMPLETE
      C-- CALL FR7CMS('CLRS CRN')
      C-- WRITE(8,450)
      C-- WRITE(8,880)
      C-- WRITE(8,410)
      C-- WRITE(8,890)

      C-- FORMAT STATEMENTS
      C-- RETURN
      FORMAT(1X,79H=====

```


580 FORMAT (1X,5SH SUMMARY CF SECTION, 1-IRD AND FORTH LINES OF INPUT DATA
 1 1X,25H ==> ENTER 1 = YES: 2 = NO)
 581 FORMAT (1X,3HF IT 7X,4H COVO,6X,3HP 10)
 582 FORMAT (1X,F5.1,5X,F7.6,3X,F3.1)
 590 FORMAT (//,1X,4HC FANG,2=SECOND, 3=NO), THIRD AND FORTH LINES INPUT DATA?
 1 /! FORMAT (1X,25H ==> ENTER 1 = YES: 2 = NO)
 600 FORMAT (1X,46H ==> ENTER FREE STREAM MACH NUMBER (FMACH): (R))
 610 FORMAT (1X,40H ==> ENTER YAW ANGLE IN DEGREES (YAW): (R))
 620 FORMAT (1X,46H ==> ENTER ATTACK IN DEGREES (AL): (R))
 630 FORMAT (1X,58H ==> ENTER DRAG COEFICIENT DUE TO FRICTION (CDO
 1): (R)), 15X,48H (UNLESS OTHERWISE AVAILABLE C01 IS RECOMMENDED)
 640 FORMAT (1X,33H SUMMARY OF FIFTH LINE INPUT DATA?,/1X,25H ==> ENTER
 1 1 = YES: 2 = NO)
 641 FORMAT (1X,5HF MACH, 5X,2HYA,8X,2HAL,8X,3FCDO)
 642 FORMAT (1X,2*6X,F3.1,7X,F8.6//)
 650 FORMAT (1X,29H CHANGE FIFTH LINE INPUT DATA?./,1X,25H ==> ENTER 1 =
 1 YES: 2 = NO)
 660 FORMAT (1X,52H ==> ENTER WING PLANFORM SYMMETRY TRIGGER, (ZSYM): (R))
 1 7X,41H,0 = YAWED WING HAS SPANWISE SYMMETRY
 2HEPT WING HAS SPANWISE SYMMETRY
 670 FORMAT (1X,78H ==> ENTER NUMBER OF SECTIONS WHERE WING SECTION GEOM
 1TRY IS DEFINED (FNS): (R),/5X,53F (VALUE MUST BE > QR = 3.0, BUT
 2NOT GREATER THAN 11) OR LEADING EDGE SWEET ANGLE IN DEGREES (SWEET
 1): (R))
 680 FORMAT (1X,58H ==> ENTER DIHEDRAL ANGLE IN DEGREES (DIHED): (R))
 690 FORMAT (1X,48H ==> ENTER FUSELAGE RADIUS (FUS): (R),/5X,33HNOTE: U
 700 FORMATE FGR,33H SUMMARY OF SIXTH LINE INPUT DATA?./,1X,25H ==> ENTER
 1 FORMATE FGR,33H SUMMARY OF SIXTH LINE INPUT DATA?./,1X,25H ==> ENTER
 710 1 YES: 2 = NO)
 711 FORMAT (1X,4HZ SYM,6X,3HFNS,7X,5HSWEET,5X,5SWEET,5X,3HFUS)
 712 FORMAT (1X,F3.1,7X,F4.1,6X,F6.3,4XF6.2,4X,5X,3HFUS)
 65X,36H ==> ENTER DIHEDRAL ANGLE IN DEGREES (DIHED): (R))
 720 FORMAT (1X,29H CHANGE SIXTH LINE INPUT DATA?./,1X,25H ==> ENTER 1 =
 1 YES: 2 = NO)
 730 FORMAT (15X,66H THE NEXT SET OF INPUT DATA WILL BE REPEATED FOR EACH
 1 WING SECTION //5X,63H AND Y COORDINATES DEFINING THE WING SECTI
 2 ON SHAPE AND PRGCE EDING ARCCUND//5X,67H STARTING WITH THE UPPER SURFACE TRAIL
 3ING EDGE AND PRGCE EDING ARCCUND//5X,35H THE LOWER SURFACE TRAIL
 4NG EDGE //5X,57H AND Y COORDINATES ARE NORMALIZED WITH THE CHORD
 5 LENGTH //5X,46H WING SECTION DEFINING COORDINATES CAN BE INPUT,/

6 5X,36H THEY THE USER OR SECTION NENU***, //6X,34H = USER INPUT SECT
 730 1ION COCFD //28X,23H** WING SECTION NENU***, //6X,19H = FLAT PLATE DATA //,6X,49H = SYMMETRICA
 2L WING COCFD //1X,DATA //,6X,19H = FLAT PLATE DATA //,6X,49H = SYMMETRICA
 3 (CAMBERED (11% THICKNESS AT 30% CHORD) //32% CHORD //,6X,51H = NACA 24-30 (CA
 4MBERED (12% THICKNESS AT 30% CHORD) //,6X,52H5 = F14 WING (CAMBERED,
 59.5% THICKNESS AT 37% CHORD) //,6X,66H = A-7 WING (CAMBERED,
 620% CHRD, 7% THICKNESS AT 43% CHORD) //,6X,64H = LISSAMAN 7769 AI

7RFCIL (CAMBERED) 1.12 THICKNESS AT 3C% CHORD) / / 6X.55H8 = NACA 0010
 8 (SYMMETRICAL 1.0% THICKNESS AT 30% CHORD) / / 6X.58H9 = NACA 0010-3
 94 (SYMMETRICAL 1.0% THICKNESS AT 40% CHORD) / / 5X.59H10 = NACA 0010
 >-3 (SYMMETRICAL 1.0% THICKNESS AT 50% CHORD) / / 5X.59H11 = NACA 00
 110-64 (SYMMETRICAL 1.0% THICKNESS AT 40% CHORD) / / 5X.59H12 = NACA
 1200 10-66 (SYMMETRICAL 1.0% THICKNESS AT 50% CHORD) / / 5X.59H13 = NAC
 3A 14-00 (SYMMETRICAL 1.0% THICKNESS AT 35% CHORD) / / 5X.58H14 = NAC
 4A 63-01 (SYMMETRICAL 1.0% THICKNESS AT 40% CHORD) / / 5X.58H15 = NA
 5CA 63-A010 (SYMMETRICAL 1.0% THICKNESS AT 35% CHORD) / / 5X.58H16 = N
 6ACA 64-C10 (SYMMETRICAL 1.0% THICKNESS AT 40% CHORD) / / 5X.58H17 =
 7NACA 64-010 (SYMMETRICAL 1.0% THICKNESS AT 40% CHORD) / / 5X.58H18 =
 8 FORMAT (5X.58H19 = NACA 65A010 (SYMMETRICAL 1.0% THICKNESS AT 40%
 1 CHORD) / / 5X.58H20 = NACA 66-010 (SYMMETRICAL 1.0% THICKNESS AT 45%
 2 CHORD) / /
 750 FORMAT (1X,35H==> ENTER DESIRED NUMBER FROM MENU!
 760 FORMAT (15X,22H** WING SECTION NUMBER! 12.1X,13H PARAMETERS** , / , 5X,
 142HNOTE: ALL DIMENSIONS MUST BE IN SAME UNITS!)
 770 1 FORMAT (1X,60H==> ENTER SECTION NUMBER FOR THIS SECTION (R)
 1ZS: (R)
 780 1 FORMAT (1X,53H==> ENTER SECTION LEADING EDGE X COORDINATE (XL): (R
 1) 1 FORMAT (1X,53H==> ENTER SECTION LEADING EDGE Y COORDINATE (YL): (R
 1) 1 FORMAT (1X,43H==> ENTER SECTION CHORD LENGTH (CHORD): (R)
 800 FORMAT (1X,55H==> ENTER SECTION THICKNESS SCALING FACTOR (THICK):
 810 1 (R)
 820 FORMAT (1X,50H==> ENTER SECTION TWIST ANGLE IN DEGREES (AT): (R)
 830 1 Y (FSEC): (R) / 1X.40H1.0 = DEFINE A NEW WING SECTION GEOMETRY FROM PREVIOUS S
 12X.67H0.C = COPY THE WING SECTION DEFINITION MUST CENTER 1.0!
 3 SECTION, / / 7X.38NOTE: FOR FIRST SECTION WHETHER OR NOT ! 5X43H
 1 THE WING SECTION IS SYMMETRICAL (YSYM): (R) / , 1X.20H0.0 = NCNSYMM
 840 2TRICAL SELECTION 1X.25H1.0 = SYMMETRICAL SECTION, / , 1X.53H NOTE: IF SYMMETRICAL SELECTION, YOU ONLY HAVE TO INPUT , / , 7X.46DEFINING POINTS FOR THE SECTION UPPER SURFACE.)
 4HE SECTION (1X,58H==> ENTER NUMBER OF WING SECTION DEFINING POINTS (FN
 850 1) : (R) * / 1X.38HNOTE: MAXIMUM NUMBER OF POINTS IS 161.
 860 1 ** * / 1 FORMAT (17X,22H** WING SECTION NUMBER, 12.1X,22H AND Y COORDINATES
 870 1 FORMAT (1X,67H==> ENTER WING SECTION DEFINING POINT X AND Y COORD.
 880 1 (XPYP): (R) /
 1 FORMAT (5X,64H THREE ADDITIONAL DATA LINES WILL BE AUTOMATICALLY WR
 1 ITED TO THE / 5X.43H BOTTOM OF YOUR INPUT FILE. THESE LINES ARE: , /
 2 5X.18HEND OF CALCULATION, / 5X.3HENX , / 5X.3TO.0!
 1 <FILE TYPE> FLG27, / 5X,69HDAT IS COMPLETE. THE INPUT DATA IS WRITTEN TO YOUR <FILE NAME
 1 > DIS

2K IF YOU WISH TO MAKE FURTHER CHANGES TO YOUR INPUT DATA
 3SI AND XEDIT THE CREATED DATA FILE //FILE, 6H TO RUN THE POTENTIAL
 4FLC PROGRAM (FLO27) USING YOUR DATA FILE //FILE, 5X, 61H XEWS IT THE FILE
 5AND ADDITIONAL CARDS (JOB CARD ETC.) //5X, 60H HAS CUTLINED
 6INSTRUCTIONS, THEN SUBMIT THE FILE TO THE //5X, 16HBATCH PR
 7OCESSOR. //1X, 4HBYE.)

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1000 FORMAT(1X,16(A4))
1010 FORMAT(3HFNX,7X,3HFNY,7X,3HFNZ,7X,5HFNESH,5X,5HFPLCT)
1020 FORMAT(F5.1,5X,F4.1,6X,F4.1,6X,F3.1,7X,F3.1)
1030 FORMAT(3HF1.1,5X,F4.1,6X,F3.1,7X,F3.1)
1040 FORMAT(3HF1.1,5X,F7.0,6X,F3.1)
1050 FORMAT(5HEMAC,5X,2HYA,8X,2HAL,8X,3HCCG)
1060 FORMAT(F4.2,6X,F3.1,7X,F3.1,7X,F8.6)
1070 FORMAT(4H2SYM,6X,3HFNS,7X,5HSWEET,5X,5HFUS)
1080 FORMAT(F3.1,7X,F4.1,6X,F6.3,4X,F10.6)
1090 FORMAT(2H2S,8X,2HXL,8X,2HYL,8X,5HCHRD,5X,5HTHICK,5X,
1100 12HAT,8X,4FFSEC)
1110 FORMAT(1(FE,4,2X),F3.1)
1120 FORMAT(2LFN)
1130 FORMAT(F5.1)
1140 FORMAT(5HXP(1),5X,5HYP(1))
1150 FORMAT(6F10.7)
1160 FORMAT(1X,18H END CF CALCULATION)
1170 FORMAT(2LFN)
1180 FORMAT(F3.1)
1190 FORMAT(14HV/ EXEC FLC27, *)
1200 FORMAT(117H// GO.SYSIN DD *)
1210 FORMAT(2H/*)
1220 FORMAT(2H//)
1230 ENC
  
```


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